



# John Cootes Site 246-264 Woodville Road, Merrylands Transport Impact Assessment

 Client //
 Wiltex Wholesale Pty Limited

 Office //
 NSW

 Reference //
 15S1396000

 Date //
 09/10/15

# John Cootes Site

# 246-264 Woodville Road, Merrylands

# Transport Impact Assessment

Issue: C 09/10/15

Client: Wiltex Wholesale Pty Limited Reference: 15\$1396000 GTA Consultants Office: NSW

**Quality Record** 

| Issue | Date     | Description  | Prepared By   | Checked By    | Approved By   | Signed        |
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# Executive Summary

A Planning Proposal is to be lodged with Parramatta City Council to amend the current planning controls for the site located at 246-264 Woodville Road in Merrylands. An indicative development yield for the site comprises some 590 residential apartments and 8,400sq.m of non-residential land uses, including supermarket, retail and community uses. Vehicle access to the site is proposed via a new signalised intersection to Woodville Road, as well as via two local connections to Lansdowne Street and Highland Street. The access points would be connected by a new internal public street network.

The proposed development has a DCP parking requirement to provide in the order of 1,143 car parking spaces. It is anticipated that this level of car parking will generally be provided within two basement car park levels, noting that there may be an opportunity to share some of the short-term retail and residential visitor parking demands.

It is envisaged that bicycle parking for the development will generally be provided in accordance with the requirements set out in the DCP.

The development is anticipated to generate in the order of 720 trips during the PM peak hour (including 580 new trips) and 870 trips during the Saturday lunchtime peak hour (including 700 new trips).

When developing the vehicle access strategy for the site, three options were considered for the primary vehicle access point from Woodville Road:

- via Oxford Street and Highland Street
- via a new access opposite Kimberley Street
- via Lansdowne Street

Given the level of traffic anticipated to be generated by the development it is considered most appropriate to provide a new access road rather than relying on the existing local road network for access. This was particularly pertinent given the sensitivities of the existing surrounding land uses including a primary school and traditional low density residential dwellings. Further to this it is noted that:

- The Oxford Street corridor already carries significant through traffic volumes and has limited spare capacity.
- While all turning movements are currently available at Lansdowne Street, traffic signals at this location could encourage additional through traffic between Woodville Road and Railway Terrace.
- Signalising Kimberley Street would provide improved access to the residential area east of Woodville Road, as well as a direct connection to the site and associated local shopping facilities. This would limit turning movements on/off Woodville Road for such local trips.

Whilst it is acknowledged that the future signalised intersection to the site is located relatively close to the existing Oxford Street signals, it is still considered to be offset greater than minimum requirements. Indeed, whilst the proposed intersection treatment (incorporating the downstream right turn lane at Oxford Street) is not typical, there are several examples of similar facilities throughout metropolitan Sydney. It is noted that the future signals will be coordinated with the existing signals located at Oxford Street to minimise any adverse impacts.

Based on the above the proposed access strategy is considered to balance the needs of maintaining through traffic capacity on Woodville Road, vehicles accessing the site and the amenity of surrounding residents, and as such, is considered appropriate.

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# 1. Introduction

# 1.1 Background

It is understood that a Planning Proposal is to be lodged with Parramatta City Council to amend the current planning controls for the site located at 246-264 Woodville Road in Merrylands.

The Planning Proposal seeks to rezone the site to a B4 Mixed use zone and increase the permissible height limits for the site and introduce a site specific floor space ratio. An indicative development yield for the site comprises some 590 residential apartments set above 8,400sq.m GFA of lower level non-residential land uses.

GTA Consultants (GTA) was commissioned by Wiltex Wholesale Pty Limited in February 2015 to undertake a transport impact assessment for the proposed development.

# 1.2 Purpose of this Report

This report sets out an assessment of the anticipated transport implications of the proposed development, including consideration of the following:

- i existing traffic and parking conditions surrounding the site
- ii suitability of the proposed parking in terms of supply (quantum)
- iii service vehicle requirements
- iv pedestrian and bicycle requirements
- v the traffic generating characteristics of the proposed development
- vi suitability of the proposed access arrangements for the site
- vii the transport impact of the development proposal on the surrounding road network.

### 1.3 References

In preparing this report, reference has been made to the following:

- an inspection of the site and its surrounds
- Parramatta City Council Development Control Plan (DCP) 2011
- Australian Standard/ New Zealand Standard, Parking Facilities, Part 1: Off-Street Car Parking AS/NZS 2890.1:2004
- traffic and car parking surveys undertaken for GTA Consultants as referenced in the context of this report
- plans and yield estimates for the proposed development prepared by Giles Tribe Architects, Job Reference 14073, dated 02/10/15.
- other documents and data as referenced in this report.



# 2. Existing Conditions

# 2.1 Subject Site

The subject site is located at 246-264 Woodville Road in Merrylands. The site of approximately 2.61 ha has frontages to Woodville Road, Lansdowne Road and Highland Street. The site currently is currently occupied by John Cootes Furniture outlet and a number of residential dwellings. The majority of the site is zoned as B6 Enterprise Corridor with the existing residential properties zoned R2 Low Density Residential.

The surrounding properties predominantly include residential uses, with the Granville South Public School abutting the site to the south and a number of retail uses fronting Woodville Road.

The location of the subject site and its surrounding environs is shown in Figure 2.1 and Figure 2.2.



Figure 2.1: Subject Site and Its Environs – Street Map

Basemap source: Sydway Publishing Pty Ltd



Figure 2.2: Subject Site and Its Environs – Aerial Map



Basemap source: NearMap (used under licence)

# 2.2 Road Network

### 2.2.1 Adjoining Roads

Woodville Road is classified as a State Road and is under the care and control of Roads and Maritime Services (RMS). It is aligned in a north-south direction running between Parramatta Road to the north and Hume Highway in the south. It is typically configured with dual three lane carriageways generally separated by a narrow concrete median. In the vicinity of the site it is configured with two through traffic lanes in each direction, with a southbound right turn lane (to the Oxford Street intersection) provided adjacent to the subject site. Clearway restrictions apply during the AM (6 to 10am) and PM (3 to 7pm) peak periods. Outside of these periods 'No Stopping' restrictions generally apply, with some unrestricted parking also provided. Pedestrian footpaths are provided on both sides of Woodville Road, whilst no formal bike facilities are provided.

The speed limit along Woodville Road is generally 70km/h, with a number of 40km/h school speed zones also provided along its length (including one for Granville South Public School located immediately south of the site).



Advice from RMS indicates that Woodville Road carries approximately 40,000 vehicles per day (vpd). Historically traffic volumes on Woodville Road peaked at 45,000vpd, but have plateaued at their current level following the opening of the M7 Motorway which provides a broader alternate route for vehicles travelling north-south in this vicinity.

A summary of the average peak hour vehicle speeds along the length of the corridor is provided in Table 2.1. The results indicate that there is significant congestion along the corridor during peak periods,

| Table 2.1: | Woodville Road | Average | Vehicle | Speeds [1] |
|------------|----------------|---------|---------|------------|
|------------|----------------|---------|---------|------------|

| Location       | Average Vehicle Speed |                |  |  |
|----------------|-----------------------|----------------|--|--|
| Location       | AM Peak Period        | PM Peak Period |  |  |
| Woodville Road | 34km/h                | 28km/h         |  |  |

[1] Provided by RMS at a project meeting dated 17 June 2014.

Oxford Street, Lansdowne Street and Highland Street are local roads provided in the vicinity of the site. Oxford Street is a collector road and includes a signalised intersection at Woodville Road and a grade separated crossing of the railway line to the west of the site.

Highland Street is currently a 'dead-end' street (hammerhead treatment) and primarily provides vehicle access to the adjacent residential properties and the Granville South Public School. Highland Street currently carries 500vpd<sup>[1]</sup>. On-street car parking demands are high on Highland Street during school times and particularly during the peak pick up and drop off periods for the primary school.

Lansdowne Street forms an east-west link between Woodville Road and Railway Terrace. There are a number of Local Area Traffic Management (LATM) treatments on Lansdowne Street, including traffic islands and road narrowings that seek to reduce vehicle speeds on Lansdowne Street. Lansdowne Street currently carries 1,500vpd<sup>[2]</sup>.

Woodville Road, Oxford Street, Highland Street and Lansdowne Street are shown in Figure 2.3 to Figure 2.6.

Figure 2.3: Woodville Road – Looking South







<sup>&</sup>lt;sup>[2]</sup> Based on peak hour traffic counts commissioned by GTA in May 2015 and assuming a peak-to-daily ratio of 10%.



<sup>&</sup>lt;sup>[1]</sup> Based on week-long tube counts on Highland Street (approximately 50m north of Oxford Street) undertaken between 9 and 16 May 2015.

Figure 2.5: Highland Street – Looking South

#### Figure 2.6: Lansdowne Street – Looking West





### 2.2.2 Surrounding Intersections

The following intersections currently exist in the vicinity of the site:

- Woodville Road / Lansdowne Street / Earl Street (priority controlled offset X-intersection)
- Woodville Road / Kimberley Street (priority controlled T-intersection)
- Woodville Road / Oxford Street (signalised T-intersection)
- Oxford Street / Highland Street (priority controlled T-intersection).

# 2.3 Traffic Volumes

GTA Consultants commissioned traffic movement counts at the immediate Woodville Road intersections during the following peak periods:

- Wednesday 13 May 2015 between 7:00 to 9:00am and 4:00 to 6:00pm
- Saturday 16 May 2015 at between 10:00am to 1:00pm.

Supplementary traffic movement counts were undertaken on Oxford Street at Highland Street (weekday only) and Woodville Road on Thursday 21 May and Saturday 23 May 2015. The additional counts were undertaken as a result of comments made by the Granville South Public School Parents and Citizens Association at the community consultation session held at the John Cootes Furniture Warehouse on Wednesday 13 May 2015 at 6pm.

The weekday AM and PM and Saturday lunchtime peak hour traffic volumes are summarised in Figure 2.7, Figure 2.8, and Figure 2.9 respectively, with full results contained in Appendix A.





Figure 2.7: Existing Weekday AM Peak Hour Traffic Volumes [1]

 The traffic counts at the Woodville Road / Oxford Street and Oxford Street/ Highland Street intersections were undertaken on Thursday 21 May 2015.





Figure 2.8: Existing Weekday PM Peak Hour Traffic Volumes [1]

 The traffic counts at the Woodville Road/ Oxford Street and Oxford Street / Highland Street intersections were undertaken on Thursday 21 May 2015.





Figure 2.9: Existing Saturday Lunchtime Peak Hour Traffic Volumes [1, 2]

[1] The traffic counts at the Woodville Road/Oxford Street intersection were undertaken on Saturday 23 May 2015.

[2] Saturday traffic counts were not undertaken of the Oxford Street/Highland Street intersection as the capacity concerns at this intersection relate to school traffic, which is not an issue on weekends.

### 2.3.1 Intersection Operation

The operation of the key intersections within the study area have been assessed using SIDRA INTERSECTION<sup>[3]</sup>, a computer based modelling package which calculates intersection performance.

The commonly used measure of intersection performance, as defined by the RMS, is vehicle delay. SIDRA INTERSECTION determines the average delay that vehicles encounter and provides a measure of the level of service.



<sup>&</sup>lt;sup>[3]</sup> Program used under license from Akcelik & Associates Pty Ltd.

Table 2.2 shows the criteria that SIDRA INTERSECTION adopts in assessing the level of service.

| Level of Service<br>(LOS) | Average Delay per vehicle (secs/veh) | Traffic Signals, Roundabout                                      | Give Way & Stop Sign                      |  |  |  |  |
|---------------------------|--------------------------------------|--|---|--|--|--|--|
| A                         | Less than 14                         | Good operation   | Good operation                            |  |  |  |  |
| В                         | 15 to 28                             | Good with acceptable delays and spare capacity                   | Acceptable delays and spare capacity      |  |  |  |  |
| С                         | 29 to 42                             | Satisfactory   | Satisfactory, but accident study required |  |  |  |  |
| D                         | 43 to 56                             | Near capacity  | Near capacity, accident study required    |  |  |  |  |
| E                         | 57 to 70                             | At capacity, at signals incidents<br>will cause excessive delays | At capacity, requires other control mode  |  |  |  |  |
| F                         | Greater than 70                      | Extra capacity required  | Extreme delay, major treatment required   |  |  |  |  |

Table 2.2: SIDRA INTERSECTION Level of Service Criteria

Table 2.3 presents a summary of the existing operation of each of the intersections in the vicinity of the site, with full results presented in Appendix B of this report (including operating conditions by intersection approach). It is noted that each of the intersections have been modelled in isolation.

| Intersection                        | Peak<br>Hour | Degree of<br>Saturation (DOS) | Average Delay<br>(sec) | 95th Percentile<br>Queue (m) | Level of Service<br>(LOS) |
|-------------------------------------|--------------|-------------------------------|------------------------|------------------------------|---------------------------|
| Woodville Road/                     | AM           | 1.0                           | 3                      | 23                           | А                         |
| Lansdowne Street                    | PM           | 1.0                           | 4                      | 22                           | А                         |
| [1]                                 | Sat          | 1.0                           | 4                      | 24                           | А                         |
|                                     | AM           | 0.48                          | 0                      | 2                            | А                         |
| Woodville Road/<br>Kimberley Street | PM           | 0.78                          | 2                      | 25                           | А                         |
| Kimbolioy shool                     | Sat          | 0.43                          | 1                      | 7                            | А                         |
|                                     | AM           | 0.91                          | 37                     | 412                          | С                         |
| Woodville Road/<br>Oxford Street    | PM           | 0.94                          | 44                     | 437                          | С                         |
|                                     | Sat          | 0.86                          | 33                     | 316                          | С                         |
| Oxford Street/                      | AM           | 0.48                          | 4                      | 40                           | А                         |
| Highland Street                     | PM           | 0.61                          | 8                      | 94                           | A                         |

Table 2.3: Existing Operating Conditions

[1] The DOS results reflect the existing delays experienced by drivers on the west approach to the intersection. The through traffic on Woodville Road is not delayed by this intersection.

Table 2.3 indicates that generally each of the nominated intersections currently operates satisfactorily with manageable queues and delays on all approaches. It is noted that as a result of the heavy through movements on Woodville Road, there are significant delays for vehicles turning right from Lansdowne Street into Woodville Road, hence a DOS of 1.00 for the west approach at this intersection (i.e. at capacity). This is consistent with on-site observations at the Woodville Road/ Lansdowne Street intersection.

It is further noted that southbound queues from the Woodville Road/ Oxford Street intersection often extend beyond the Kimberley Street and Lansdowne Street intersections, particularly during the PM peak hour. Similarly, northbound queues were observed to extend a significant distance to the south of the Woodville Road/ Oxford Street intersection during the AM peak hour.

The modelling indicates that during the road network peak hours, the Oxford Street/Highland Street intersection operates with a satisfactory level of service. However, the traffic volumes indicate increased activity to and from Highland Street during peak school pick-up and drop-off



periods. During the peak 15 minute periods at 8:45am and 3:00pm, there was a three-fold increase in traffic accessing Highland Street. During these periods there was increased queuing and delays, beyond those presented in Table 2.3, on Highland Street.

# 2.4 Existing Travel Characteristics

### 2.4.1 ABS Data: Journey to Work

The NSW Bureau of Transport Statistics (BTS) is responsible for collating and analysing transport related data for the state, including census data collected by the Australian Bureau of Statistics. The smallest geographical area that travel data is available is a Travel Zone (TZ).

The ABS data has been sourced for the two nearest travel zones to the site (1229 and 1250) and are illustrated in Figure 2.10.





(Source: <u>http://www.bts.nsw.gov.au/</u>)

#### Employees of Study Area

Of the trips travelled by the employed population within these Travel Zones, 83% are by private vehicle, either as the driver or passenger. Travelling by public transport (train and bus services) accounts for only 5% of trips while 6% of people walked to work.



According to the 2011 Census, 49% of the employed population within the nominated Travel Zones live in the same area (Merrylands-Guildford). This indicates that many of the trips to/from work based in this area are local trips.

Figure 2.11 and Figure 2.12 illustrate the most popular origin locations and modes of transportation used to travel to work within the nominated TZs.

Figure 2.11: Top Ten Ranking Origin Locations



Source: Bureau of Transport Statistics

#### Residents of Study Area



Figure 2.12: Methods of Transport from Origin

Locations



Of the employed residents in the nominated Travel Zones 20% work in the same area (Merrylands-Guildford). In addition, 75% of residents commute to work by private vehicle, either as a driver or passenger, while 21% travelled by public transport (train and bus services).

Figure 2.13 and Figure 2.14 show the full list of destination locations and modes of transportation used by employed residents of the nominated TZs to travel to work.

#### Figure 2.13: Top Ten Ranking Destination Locations

| - C.       | No. | Destination or place of work (SA3) |
|------------|-----|------------------------------------|
|            | 162 | Merrylands - Guildford             |
|            | 109 | Parramatta                         |
|            | 107 | Sydney Inner City                  |
| 1          | 51  | Auburn                             |
| Ū.,        | 50  | No fixed place of work             |
| 1          | 34  | Strathfield - Burwood - Ashfield   |
| - Û        | 33  | Fairfield                          |
| 1          | 29  | Bankstown                          |
| 1          | 27  | Chatswood - Lane Cove              |
| - <b>.</b> | 25  | Carlingford                        |
|            | 193 | Other                              |

Figure 2.14: Methods of Transport to Destination Locations



Source: Bureau of Transport Statistics

Comparison to Metropolitan Sydney

A summary of the results for the above TZs has been benchmarked against all Sydney Greater Metropolitan Region (GMR) employees and residents and is summarised in Table 2.4.



| Mode                                | Study     | Sydney GMR |                              |
|-------------------------------------|-----------|------------|------------------------------|
|                                     | Residents | Employees  | (Employees and<br>Residents) |
| Vehicle<br>(as driver or passenger) | 73%       | 83%        | 72%                          |
| Public Transport<br>(bus or train)  | 21%       | 5%         | 20%                          |
| Walk or Cycle                       | 1%        | 6%         | 4%                           |
| Other                               | 5%        | 6%         | 4%                           |

#### Table 2.4: Comparison of ABS Journey to Work Data

[2] Includes BTS Travel Modes 1229 and 1250.

Table 2.4 indicates that residents have a comparable mode share to the Sydney GMR, whilst employees have a greater reliance on private vehicle travel (83% v 72%) and a lower use of public transport (5% v 20%) compared to the Sydney GMR.

### 2.4.2 ABS Data: Car Ownership

ABS car ownership data has been collated for the study area, including the suburbs of Merrylands and Guildford (noting that the site is on the border of both suburbs).

A summary of the car ownership data for existing residents (for dwellings in apartment buildings) from the 2011 ABS is summarised below:

- Studio apartments: 0.16 (sample size of 31 apartments)
- 1-bedroom apartments: 0.52 (sample size of 306 apartments)
  - 1.00 (sample size of 3,114 apartments)
- 2-bedroom apartments:
   3-bedroom apartments:
- 1.29 (sample size of 3,114 dpdrimeril.
- 3-bedroom apartments:
- 1.39 (sample size of 368 apartments)

It is further noted that 24% of residents of existing studio, 1, 2 and 3-bedroom apartments do not own a car.

# 2.5 Woodville Road Urban Design Study (Draft)

Roberts Day, on behalf of Parramatta City Council, is currently preparing the Woodville Road Urban Design Study that looks at potential options to regenerate development along the Woodville Road corridor. The study has yet to be finalised.

### 2.6 Sustainable Transport

#### 2.6.1 Public Transport

The following public transport facilities are provided in the vicinity of the site:

- Buses on Woodville Road (<100m from the site)
- Buses on Excelsior Street (400m east of the site)
- Merrylands Railway Station (1.7km northwest of the site)
- Guildford Railway Station (1.7km southwest of the site)

The nearby public transport facilities are illustrated in Figure 2.15.



Figure 2.15: Surrounding Public Transport Facilities

A review of the public transport services available in the vicinity of the site is summarised in Table 2.5.

| Station Name                 | Bus Service / Rail<br>Line                                     | Frequency of<br>Services             | Walking<br>Distance to<br>Site | Pedestrian/Cyclist Links  |
|------------------------------|--|--------------------------------------|--------------------------------|---|
| Woodville Road Bus<br>Stop   | 907  | Every 20 – 30<br>minutes             | <100m<br>(2 minutes)           | Pedestrian footpaths<br>provided  |
| Excelsior Street Bus<br>Stop | 906<br>908   | Every 30 minutes<br>Every 60 minutes | 400m<br>(5 minutes)            | Pedestrian footpaths<br>provided on Earl Street   |
| Guildford                    | T2 Airport, Inner West<br>and South Line<br>T5 Cumberland Line | Every 15 minutes                     | 1.7km<br>(20 minutes)          | Pedestrian footpaths and on-<br>road bicycle lanes are<br>provided in each direction<br>on Guildford Road       |
| Merrylands                   | T2 Airport, Inner West<br>and South Line<br>T5 Cumberland Line | Every 15 minutes                     | 1.7km<br>(20 minutes)          | Pedestrian footpaths and<br>wide kerbside lane provided<br>for cyclists in each direction<br>on Merrylands Road |

 Table 2.5:
 Public Transport Provision

In addition, it is noted that Woodville Road may in the future cater for light rail services connecting Parramatta to Bankstown or alternatively could cater for a rapid bus route.

### 2.6.2 Pedestrian Infrastructure

Pedestrian footpaths are provided on both sides of Woodville Road, Oxford Street and Highland Street (abutting the school). Pedestrian paths are provided on the north side of Lansdowne Street (but do not extend to Railway Terrace) and are not typically provided on Kimberley Street.

A signalised pedestrian crossing of Woodville Road is provided on the north side of the Woodville Road/ Oxford Street intersection.

A shared path is provided along Railway Terrace and provides a connection to Merrylands and Guildford Railway Stations.

### 2.6.3 Cycle Infrastructure

Limited cycle facilities are currently provided in the vicinity of the site.

### 2.6.4 Local Car Sharing Initiatives

There are currently no car sharing pods located in reasonable walking distance of the site.



# 3. Development Proposal

# 3.1 Land Uses

The Planning Proposal seeks to rezone the subject site from B6 Enterprise Corridor and R2 Low Density Residential to a B4 Mixed Use zoning and permissible Floor Space Ratio of 2.24:1. Specifically, the proposal includes the construction of a number of buildings set around a central square. The buildings range from 3 to 12 storeys and include a combination of all residential and mixed uses.

A summary of the indicative land uses (subject to change) are provided in Table 3.1.

| Land Use        | Description                           | Size                                 |  |  |
|-----------------|---------------------------------------|--------------------------------------|--|--|
|                 | 1-bedroom                             | 148 dwellings                        |  |  |
| Residential     | 2-bedroom                             | 383 dwellings                        |  |  |
| Residentia      | 3-bedroom                             | 59 dwellings                         |  |  |
|                 | Total                                 | 590 dwellings                        |  |  |
| Non-Residential | Supermarket, Retail and Community Use | 8,362sq.m GFA<br>(6,833sq.m NLA) [1] |  |  |

Table 3.1: Indicative Development Schedule

[1] Incorporating 3,000sq.m NLA supermarket and 3,833sq.m NLA of retail and community uses.

# 3.2 Vehicle Access

Vehicle access to the future land uses is proposed to be provided via a new internal road network. The internal road network would connect to the surrounding existing road network as follows:

- Signalised intersection to Woodville Road
- Priority controlled intersection to Lansdowne Street
- Continuation of Highland Street

It is proposed to provide vehicle access to the each of the buildings from the internal road network as well as to Highland Street. No direct site vehicle access is proposed from Woodville Road or Lansdowne Street.

The three existing driveways from Woodville Road to the subject site would be removed.

When developing the vehicle access strategy for the site, three options were considered for the primary vehicle access point from Woodville Road:

- via Oxford Street and Highland Street
- via a new access opposite Kimberley Street
- via Lansdowne Street

Given the level of traffic anticipated to be generated by the development it is considered most appropriate to provide a new access road rather than relying on the existing local road network for access. This was particularly pertinent given the sensitivities of the existing surrounding land uses including a primary school and traditional low density residential dwellings. Further to this it is noted that:

• The Oxford Street corridor already carries significant through traffic volumes and has limited spare capacity.



- While all turning movements are currently available at Lansdowne Street, traffic signals at this location could encourage additional through traffic between Woodville Road and Railway Terrace.
- Signalising Kimberley Street would provide improved access to the residential area east of Woodville Road, as well as a direct connection to the site and associated local shopping facilities. This would limit turning movements on/off Woodville Road for such local trips.

Based on the above the proposed access strategy is considered to balance the needs of maintaining through traffic capacity on Woodville Road, vehicles accessing the site and the amenity of surrounding residents, and as such, is considered appropriate.

Further discussion regarding the proposed intersection and vehicle access arrangements are provided in Section 5 of this report.

# 3.3 Car Parking

Car parking would generally be provided in basement car parking areas (typically 2 levels). The basement car parking would be complemented by on-street car parking to be provided on the new internal road network.

The provision of car parking is not yet known, however, car parking would be provided generally in accordance with the current Parramatta Council DCP requirements (refer to Section 4).

# 3.4 Pedestrian and Bicycle Facilities

As part of the development it is proposed to develop an active travel corridor along Lansdowne Street between the site and Railway Terrace. This would provide an improved pedestrian and cyclist connection between the site and Merrylands Railway Station.

### 3.5 Overview

An overview of the key transport components of the proposal are presented in Figure 3.1.







# 4. Parking Assessment

# 4.1 Car Parking

### 4.1.1 DCP Requirements

The car parking requirements for different development types are set out in Parramatta City Council DCP (Section 3.6.2). A review of the car parking rates and the floor area schedule results in a DCP parking requirement for the proposed development as summarised in Table 4.1. For assessment purposes, all the non-residential floor area has been assumed to be a generic retail land use.

| Description | Use Size / No. DCP Pc                         |                                  | DCP Parking Rate         | DCP Parking<br>Requirement |  |  |  |
|-------------|---|----------------------------------|--------------------------|----------------------------|--|--|--|
|             | 1-bedroom 148 dwellings 1 space per dwelling  |                                  | 148                      |                            |  |  |  |
| Desidential | 2-bedroom                                     | 383 dwellings                    | 1.25 spaces per dwelling | 479                        |  |  |  |
| Residential | 3-bedroom                                     | 59 dwellings                     | 1.5 spaces per dwelling  | 89                         |  |  |  |
|             | Visitor                                       | 590 dwellings                    | 0.25 spaces per dwelling | 148                        |  |  |  |
| Retail      | Refer to uses indicative<br>uses in Table 3.1 | 8,362sq.m GFA<br>(6,833sq.m NLA) | 1 space per 30sq.m GFA   | 279                        |  |  |  |
|             | Total   |                                  |                          |                            |  |  |  |

Table 4.1: DCP Car Parking Requirements

Based on the above, the proposed development is required to provide in the order of 1,143 car parking spaces, subject to the make-up of the final land uses. It is noted that a visitor parking rate of 0.25 spaces per dwelling would typically be applied to smaller developments and represents a significant number of parking spaces in this instance. Future Development Application(s) for the site would need to justify any proposed visitor parking reduction.

# 4.1.2 Potential Car Parking Reductions

The provision of future car parking has not yet been determined and will be confirmed as part of any subsequent Development Application should the Planning Proposal be approved. Notwithstanding, it is envisaged that any future development on the rezoned lands would provide car parking generally in accordance with the DCP parking requirement presented above. However, there may be an opportunity to provide a shared car parking pool for the retail and residential visitor parking demands. In this regard, it is noted that residential visitor demands typically peak in the evening, whilst retail demands typically peak during the day. More specifically, it is commonly accepted that daytime residential visitor demands are 50% of the evening demands.

Therefore it could be appropriate that a reduction (based on a temporal profile of car parking demand) in residential visitor car parking could be applied.

Whilst not specifically required under the DCP, the provision of car share spaces (e.g. GoGet or similar) on-site in place of resident and/or visitor spaces should be considered. Industry evidence suggests a single car share space can replace the need for around 5 parking spaces for residents and/or visitors.



# 4.2 Active Transport

## 4.2.1 Bicycle Parking

Bicycle parking for the site should be provided in accordance with the requirements of the Parramatta City Council DCP 2011 (Section 3.6.2), as summarised in Table 4.2. The actual number of bicycle spaces to be provided may alter when the mix of non-residential land uses are refined at the Development Application stage.

#### Table 4.2: Bicycle Parking Requirements

| Use         | Size          | DCP Bicycle Parking<br>Rate [1] | Bicycle Parking<br>Requirement |
|-------------|---------------|---------------------------------|--------------------------------|
| Residential | 590 dwellings | 1 space per 2 dwellings         | 295 spaces                     |
| Retail      | 8,362sq.m GFA | 1 space per 200sq.m GFA         | 42 spaces                      |
|             | 337 spaces    |                                 |                                |
|             |               |                                 |                                |

[1] Sourced from Section 3.6.2 of the Parramatta City Council DCP 2011.

Table 4.2 indicates that any future development of the John Cootes site (based on the indicative yield) should provide approximately 337 bicycle spaces.

# 4.2.2 Cyclist and Pedestrian Access

Cyclist and pedestrian access to the new uses would be provided from the future internal road network as well as from the surrounding road network, including Woodville Road, Lansdowne Road and Highland Street. In addition a new active transport corridor on Lansdowne Road connecting the site to Railway Terrace (which in turn provides access to both Merrylands and Guildford Railway Stations) would be beneficial in promoting local and regional active travel.

The form of the potential active transport corridor has not yet been determined, but could include a continuation of the existing footpath with an on-road mixed traffic bicycle facility, an off-road shared path, a separated cycleway or similar. The make-up of the future facility would need to be determined in consultation with Council and local residents as part of the Development Application stage.

The facility would encourage residents, customers and employees of the development to walk or cycle between the site and nearby transport nodes or the Merrylands Town Centre.

# 4.3 Loading Arrangements

The loading provision requirements for different development types are set out in Parramatta City Council DCP (Section 3.6.2). The DCP requires that one loading bay be provided for every 400sq.m GFA of retail floor area. Application of this rate indicates that the site would have a requirement to provide 21 loading bays to service the proposed retail land uses.

Whilst the number of loading bays for the development has not yet been determined, the provision of 21 loading bays is considered excessive for a development of this size and a dispensation of the number of loading bays to be provided will likely be sought at the Development Application stage.

All loading vehicle access will be provided from the internal road network to the site. All loading vehicles would access the site via the signalised intersection from Woodville Road or Lansdowne Street (from Woodville Road), depending on vehicle size, internal access design and final internal

road geometry. Heavy vehicles would not be permitted to use Highland Street or Lansdowne Street further west, with physical constraints expected to be provided to discourage such activity.

# 4.4 Green Travel Plan

The Objective of a Travel Plan as defined in the DCP (2011) is reproduced below:

"To reduce car trips and encourage the use of sustainable transport."

A Travel Plan is not technically required for the site, noting that whilst the site exceeds 5,000sq.m of gross floor area, it is located greater than 800m radial distance from a Railway Station.

Notwithstanding, it is recommended that a Travel Plan be prepared at the Development Application stage and would include the following (as per the requirements of the DCP):

- mode share targets including a reduction in single vehicle trips
- travel data estimates of future trip to and from the site
- measures to achieve the mode share targets.



# 5. Traffic Impact Assessment

# 5.1 Traffic Generation

### 5.1.1 Residential Land Uses

Having consideration for a range of factors including the size of units and the site location, Table 5.1 sets out traffic generation estimates for both peak hour and daily periods. It is noted that the upper range of the residential yield has been adopted to present a conservative assessment.

Table 5.1: Estimated Development Traffic Generation

| A               | No. of Dwellings        |  | eration Rates                        | Traffic Generation Estimates       |                                     |  |
|-----------------|-------------------------|--|--------------------------------------|------------------------------------|-------------------------------------|--|
| Access          | Access No. of Dwellings | Peak Hour [1]                          | Daily                                | Peak Hour                          | Daily                               |  |
| To/from carpark | 590                     | 0.4 vehicle<br>movements /<br>dwelling | 4 vehicle<br>movements /<br>dwelling | 236 vehicle<br>movements /<br>hour | 2,360 vehicle<br>movements /<br>day |  |

[1] Adopting a peak to daily ratio of 10%.

Table 5.1 indicates the residential component of the proposed development could be expected to generate approximately 2,360 vehicle movements per day and 236 vehicle movements during each respective peak hour on a typical weekday.

#### 5.1.2 Non-Residential Land Uses

Traffic generation estimates for the non-residential development uses have been sourced from RMS 'Guide to Traffic Generating Developments' (October 2002). A summary of the generic RMS traffic generation rates and resultant traffic generation for the supermarket and retail uses are provided in Table 5.2.

| Land Use    | Sino                 | Adopted Traffic Generation Rate<br>for Assessment |                  |       | Resultant Traffic Generation |                  |       |  |
|-------------|----------------------|---|------------------|-------|------------------------------|------------------|-------|--|
|             | Size                 | PM Peak<br>Hour                                   | Sat Peak<br>Hour | Daily | PM Peak<br>Hour              | Sat Peak<br>Hour | Daily |  |
| Supermarket | 3,000sq.m NLA        | 15.5  | 14.7             | 147.5 | 465                          | 441              | 4,425 |  |
| Retail      | Retail 3,833sq.m NLA |   | 4.6 10.7 55.5    |       | 176                          | 410              | 2,127 |  |
|             |                      | 641   | 851              | 6,552 |                              |                  |       |  |

 Table 5.2:
 RMS Non-Residential Traffic Generation Rates

Table 5.2 indicates the non-residential uses of the proposed development could be expected to generate approximately 6,550 vehicle movements per day and 640 and 851 vehicle movements during the weekday PM and Saturday lunchtime peak hours.

Whilst not yet finalised the proposed mix of land uses includes supermarket, retail, medical centre, gymnasium, child care, restaurants and communities facilities. In this regard, it is anticipated that some visitors to the site would visit more than one use at a time. Reference has been made to the RMS Guide which indicates that for centres up to 10,000sq.m GLFA a multi-purpose trip reduction factor of 25% could be applied.

Application of the multi-trip reduction factor indicates the following non-residential traffic generation:

- Weekday PM Peak Hour: 481vph
- Saturday Peak Hour: 638vph
- Daily: 4,914vpd

It is noted that the non-residential uses would be expected to generate significantly less traffic during the AM peak period than the weekday PM and Saturday lunchtime peak periods.

#### 5.1.3 Summary

A summary of the weekday PM and Saturday lunchtime peak hour and daily traffic generation for the proposed development is provided in Table 5.3.

| Land Use        | Weekd | ay PM Pe | ak Hour | Saturda | y Lunchtir<br>Hour | ne Peak | Daily |       |       |
|-----------------|-------|----------|---------|---------|--------------------|---------|-------|-------|-------|
|                 | In    | Out      | Total   | In      | Out                | Total   | In    | Out   | Total |
| Residential     | 165   | 73       | 236     | 118     | 118                | 236     | 1,180 | 1,180 | 2,360 |
| Non-Residential | 240   | 241      | 481     | 319     | 319                | 638     | 2,457 | 2,457 | 4,914 |
| Total           | 405   | 314      | 717     | 437     | 437                | 874     | 3,637 | 3,637 | 7,274 |

Table 5.3: Summary of Site Traffic Generation [1]

[1] Adopting an in / out split of 70:30 (AM) and 50:50 (Saturday) for residential and 50:50 for non-residential (PM and Saturday).

Table 5.3 indicates that the proposed development could be expected to generate in the order of 717, 874 and 7,274 movements during the weekday PM peak hour, Saturday lunchtime peak hour and daily traffic volumes, respectively.

The AM peak hour traffic generation is anticipated to be considerably less than the weekday PM and Saturday lunchtime peak hours as the non-residential uses will be generating significantly less traffic than during the other peak periods. As such, only the critical weekday PM and Saturday lunchtime peak hours have been assessed as part of the Planning Proposal assessment.

### 5.1.4 Characteristic Trip Types

An important characteristic of the traffic generation of the above uses is the different types of trips which may occur. These different trip types correspond to:

- 'Primary Trips'
- 'Link-diverted trips'
- 'Non-link-diverted trips'.

Primary trips and link-diverted trips involve a vehicle either making a special trip or a modification of the route to an existing trip. Non-link-diverted trips, on the other hand, correspond to those trips which do not involve a diversion from the route that would otherwise have been taken, or in other words are trips generated by passing traffic. The important distinction here is that it is only primary trips and link-diverted trips which impact upon the external road network. Non-link-diverted trips need to be considered in the design of access driveways, turning lanes and so on, they do not constitute additional traffic per se.

Table 5.4 had been prepared to give an indication of the relative contribution each trip type makes as a proportion of all trips accessing the use.



| Use         | Primary Trips / Link-diverted trips (%) | Non-link-diverted trips (%) |
|-------------|---|-----------------------------|
| Residential | 100%                                    | 0%                          |
| Supermarket | 72%                                     | 28%                         |
| Retail      | 72%                                     | 28%                         |

#### Table 5.4: Trip Types for the Proposed Development [1]

[2] Austroads Guide to Traffic Management Part 12: Traffic Impacts of Developments (pg. 106).

A non-link-diverted trip proportion of 28% of the non-residential traffic equates to 5% and 8% of the weekday PM and Saturday lunchtime peak hour traffic volumes on Woodville Road, respectively.

#### 5.1.5 Traffic Generation Summary

Based on the above information, Table 5.5 sets out the resultant vehicle generation for both the morning/evening peak hour and daily periods. The Table indicates that a maximum of 582 and 695 vehicle movements could be generated by the site during the PM and Saturday traffic peaks, with 5,898 additional vehicle movements generated over the entire day.

|  |               | Road Network PM<br>Peak                   |                                | Road N<br>Saturday                        | letwork<br>Peak Hour           | Daily Movements                           |                                |  |
|--|---------------|---|--------------------------------|---|--------------------------------|---|--------------------------------|--|
| Description  | Size          | Primary<br>and Link-<br>diverted<br>trips | Non-link-<br>diverted<br>trips | Primary<br>and Link-<br>diverted<br>trips | Non-link-<br>diverted<br>trips | Primary<br>and Link-<br>diverted<br>trips | Non-link-<br>diverted<br>trips |  |
| Residential  | 590 dwellings | 236                                       | 0                              | 236                                       | 0                              | 2360                                      | 0                              |  |
| Non-<br>Residential<br>(retail and<br>supermarket) | 8,362sq.m     | 346                                       | 135                            | 459                                       | 179                            | 3,538                                     | 1,376                          |  |
| Total  |               | 582                                       | 135                            | 695                                       | 179                            | 5898                                      | 1376                           |  |

Table 5.5: Traffic Generation

# 5.2 Distribution and Assignment

The directional distribution and assignment of traffic generated by the proposed development will be influenced by a number of factors, including the:

- i configuration of the arterial road network in the immediate vicinity of the site
- ii existing operation of intersections providing access between the local and arterial road network
- iii distribution of households in the vicinity of the site
- iv surrounding employment centres, retail centres and schools in relation to the site
- v likely distribution of employee's residences in relation to the site
- vi configuration of access points to the site.

Having consideration to the above, for the purposes of estimating vehicle movements, the following directional distributions have been assumed:

- to Woodville Road (via new signals): 90%
  - North: 45%
  - East: 5%
  - South: 50%



- To Woodville Road (via Lansdowne Street): 5%
- Oxford Street (via Highland Street):

Based on the above, Figure 5.1 and Figure 5.2 have been prepared to show the estimated marginal increase in turning movements in the vicinity of the subject property following full site development during the weekday PM and Saturday lunchtime peak hours, respectively.

5%.

Figure 5.1: Weekday PM Peak Hour Site Generated Traffic Volumes







Figure 5.2: Saturday Lunchtime Peak Hour Site Generated Traffic Volumes

The resultant traffic volumes (existing volumes + development volumes – passing traffic discount) for the future weekday PM and Saturday lunchtime peak hour are presented in Figure 5.3 and Figure 5.4.





Figure 5.3: Weekday PM Peak Hour Post Development Traffic Volumes





Figure 5.4: Saturday Lunchtime Peak Hour Post Development Traffic Volumes [1]

 Given that there is no regular school traffic on Saturdays, the post-development traffic volumes have not been assessed at the Oxford Street/ Highland Street intersection.

# 5.3 Proposed Intersection Works

Subject to negotiations with RMS, it is proposed to provide a new signalised intersection to Woodville Road at the existing priority controlled intersection with Kimberley Street. The new signalised intersection would be located approximately 150m north of the existing signalised intersection of Woodville Road and Oxford Street. As such, the proposed signalised intersection providing access to the site would need to be linked or coordinated with the existing signals to the south. This would minimise the likelihood that any queuing on the south approach to the new intersection extends through the existing Woodville Road/ Oxford Street intersection.



The following works are proposed to provide the new site access to Woodville Road:

- Provision of a western approach to the existing Woodville Road/ Kimberley Street intersection (incorporating two approach lanes).
- Shift the two northbound lanes to the west (within the existing kerb line).
- Provide an additional right turn lane on Woodville Road (north approach) to cater for vehicles accessing the site.
- Maintain a dedicated turn lane for traffic turning right into Oxford Street from Woodville Road through the new intersection.
- The signal timings would be linked to the existing Woodville Road/ Oxford Street signals (i.e. approximately 145 second cycle time).

A sketch of the proposed vehicle access arrangements is illustrated in Figure 5.5. If required, a short left turn (deceleration) lane could be provided on the south approach to the intersection. However, in this regard it is noted that the modelling presented below indicates that a short left turn lane would not be required.



Figure 5.5: Proposed Access Arrangements – New Signalised Intersection

Whilst it is acknowledged that the future signalised intersection to the site is located relatively close to the existing Oxford Street signals, it is still considered to be offset greater than minimum requirements. Indeed, whilst the proposed intersection treatment (incorporating the downstream right turn lane at Oxford Street) is not typical, there are several examples of similar facilities throughout metropolitan Sydney.

Further design development and consultation with RMS would be required to progress the proposed traffic signals.



# 5.4 Traffic Impact

### 5.4.1 Peak Hour Traffic

The impact of the development traffic upon the surrounding intersections has been assessed using SIDRA INTERSECTION. On the basis of the turning movement estimates presented above, Table 5.6 presents a summary of the anticipated future operation of the intersections following the full development of the site. Detailed results of this analysis are provided in Appendix B of this report. It is noted that this assessment does not take into account any changes to the background traffic volumes as a result of intensification of existing surrounding land uses. Furthermore, the intersections of Oxford Street and Kimberley Street with Woodville Road have again been modelled in isolation<sup>1</sup>. However, appropriate model configuration with respect to intersection coordination, cycle/ phase times and vehicle arrival profile have been adopted. It is recommended that as part of any Development Application for the site, more detailed modelling be undertaken that specifically accounts for the interaction between the two signalised intersections.

|                                   |              | Existing Conditions              |                        |                                 |                              | Post Development                 |                        |                                 |                              |
|-----------------------------------|--------------|----------------------------------|------------------------|---------------------------------|------------------------------|----------------------------------|------------------------|---------------------------------|------------------------------|
| Intersection                      | Peak<br>Hour | Degree of<br>Saturation<br>(DOS) | Average<br>Delay (sec) | 95th<br>Percentile<br>Queue (m) | Level of<br>Service<br>(LOS) | Degree of<br>Saturation<br>(DOS) | Average<br>Delay (sec) | 95th<br>Percentile<br>Queue (m) | Level of<br>Service<br>(LOS) |
| Woodville Road/                   | PM           | 1.0                              | 4                      | 22                              | А                            | 1.0                              | 4                      | 25                              | А                            |
| Lansdowne Street<br>[1]           | Sat          | 1.0                              | 4                      | 24                              | А                            | 1.0                              | 4                      | 24                              | А                            |
| Woodville Road/                   | PM           | 0.78                             | 2                      | 25                              | А                            | 0.76                             | 9                      | 83                              | А                            |
| Kimberley Street                  | Sat          | 0.43                             | 1                      | 7                               | А                            | 0.78                             | 11                     | 109                             | А                            |
| Woodville Road/                   | PM           | 0.94                             | 44                     | 437                             | С                            | 1.0                              | 50                     | 548                             | D                            |
| Oxford Street                     | Sat          | 0.86                             | 33                     | 316                             | С                            | 0.89                             | 34                     | 357                             | С                            |
| Oxford Street/<br>Highland Street | PM           | 0.61                             | 8                      | 94                              | А                            | 0.62                             | 10                     | 95                              | A                            |

[1] The through traffic on Woodville Road would continue not to be delayed by this intersection.

In general, Table 5.6 indicates that each of the intersections are anticipated to operate with comparable of levels of service to their existing operation. Further discussion regarding each of the intersections is provided below.

#### Woodville Road/ Lansdowne Street Intersection

The Woodville Road/ Lansdowne Street intersection is expected to operate with only minor increases to average delays and 95<sup>th</sup> percentile queues. It is noted that the right turn out of Lansdowne Street into Woodville Road is already at capacity. Additional right turning traffic is not anticipated as a result of the development, as these movements would be accommodated at the new traffic signals. Existing right turning traffic would have the opportunity to continue through the site and access the proposed new traffic signals, potentially reducing travel time delays.

<sup>&</sup>lt;sup>1</sup> The intersections are unable to be adequately modelled using the SIDRA Network function as the right turn lane from the Oxford Street intersection that extends through the proposed Kimberley Street signals is unable to be accurately coded into the program.

#### Woodville Road/ Kimberley Street/ Site Access Intersection

The proposed signalised intersection at Woodville Road and Kimberley Street is expected to operate at an acceptable Level of Service, with manageable queues and delays on all approaches. The modelling indicates that the majority of green time would be allocated to Woodville Road, hence minimising delays to the majority of traffic.

#### Woodville Road/ Oxford Street

The Woodville Road/ Oxford Street intersection is expected to operate with a LOS D during the PM peak hour (up from a LOS C) and a LOS C during the Saturday lunchtime peak hour. The Oxford Street approach would operate at capacity during the PM peak hour, noting that no additional traffic is anticipated on the Oxford Street approach from the development.

#### Woodville Road Signalised Intersections (Combined)

It is noted that the assessment of each of the signalised intersections presented above has been undertaken separately. A qualitative assessment of their combined operation has therefore been undertaken.

The proposed future signalised intersection servicing the site would be located approximately 150m north of the existing Oxford Street signals. Given the close proximity of the intersections, the signal timings would be coordinated to maximise efficiency for through vehicles on Woodville Road. The modelling undertaken above assumes that the existing cycle time observed at the Oxford Street signals of 145 seconds is provided at both intersections in the future.

Oxford Street carries greater traffic volumes compared to the proposed site access (circa 1500vph versus 800vph) and would therefore be allocated more green time than the site access and Kimberley Street at the new signals. As such, vehicles on Woodville Road would continue to be able to access the Oxford Street intersection with minimal disruption.

The signals would be coordinated to accommodate northbound (or inbound) movements in the AM peak hour and southbound (or outbound) movements in the PM peak hour. Whilst it is acknowledged that the right turn queue into Oxford Street would (at peak times) extend through the new signals, the new signals (and the continuation of the Oxford Street right turn lane through the new signals) would not restrict the right turn capacity at Oxford Street (i.e. the storage area for 20 vehicles to queue in the right turn lane prior to the new signals would not clear in each signal cycle).

There are anticipated to be up to 200 right turn movements from the site access onto Woodville Road during the peak hour or an average of about 8 vehicles each traffic signal cycle. There would therefore be sufficient storage area between the two signalised intersections to accommodate the vehicles turning right out of the site access.

Notwithstanding the above, it is recommended that the transport impact assessment report that would accompany the Development Application takes into account the detailed interaction of the two intersections (and associated impacts) once the design of the new traffic signals has progressed further.

#### Oxford Street/ Highland Street

The Oxford Street/Highland Street intersection is expected to continue to operate with comparable average delays and 95<sup>th</sup> percentile queues to its existing operation during the road network peak hours.


There are however concentrated capacity constraints at the existing Oxford Street/Highland Street intersection during peak school pick-up and drop-off periods. The peak traffic generation from the site is predicted to occur during the PM road network peak hour and the Saturday lunchtime peak hour, which would not coincide with school peak hours. However, the site would generate some traffic during these peak school periods, which may further exacerbate the congestion at the intersection.

Whilst the school peak hour congestion at the Oxford Street/Highland Street intersection is an existing constraint, it may be possible to increase the capacity and safety of this intersection as part of the development.

In this regard, GTA has reviewed a number of mitigating measures that could improve the operation of the intersection, including:

- Roundabout
- Traffic signals
- Seagull right turn treatment

As the existing capacity constraints only occur for a short period of time on a typical weekday, the review indicated that the provision of a 'seagull' right turn treatment (similar to the one provided at the Oxford Street/Harold Street intersection) would be the most appropriate treatment to improve the operation of the intersection during peak school periods. The benefit of the seagull treatment is that vehicles turning right out of Highland Street only need to initially giveway to eastbound vehicles on Oxford Street rather than vehicles in both directions as is currently the case. In addition, vehicles turning right into Highland Street would not delay westbound vehicles on Oxford Street. For reference, the existing seagull treatment at the adjacent Oxford Street/Harold Street intersection is provided in Figure 5.6.

Figure 5.6: Proposed Access Arrangements – New Signalised Intersection



Source: NearMap (used under licence, dated 6/05/15

The provision of traffic signals and/or a roundabout were investigated, however, neither treatment was consistent with other intersection treatments along the Woodville Road corridor, nor do the existing and future volumes on Highland Street warrant such treatments.

The proposed 'seagull' intersection treatment would benefit existing and future traffic accessing Highland Street.

It is noted the proposed treatment would result in the loss of a number of on-street car parking spaces which would need to be considered further by Council and local stakeholders.



#### 5.4.2 Daily Traffic

A summary of the existing, additional and post development daily traffic volumes on the surrounding local roads are provided in Table 5.7.

|                  |          | Daily Traffic Volumes |                  | Indicative                       |
|------------------|----------|-----------------------|------------------|----------------------------------|
| Location         | Existing | Additional            | Post Development | Maximum Daily<br>Traffic Volumes |
| Lansdowne Street | 1,500vpd | +300vpd [1]           | 1,800vpd         | 3,000vpd (approx.)               |
| Highland Street  | 500vpd   | +300vpd [1]           | 800vpd           | [2]                              |

Table 5.7: Daily Traffic Volume Capacity Assessment

[1] Total traffic generation multiplied by the traffic to the local road network (=5,898 x 5%).

[2] Sourced from the RMS Guide to Traffic Generating Developments (Table 4.6) and assuming each road is classified as a local street.

Table 5.7 indicates that each of the surrounding local roads is anticipated to operate within the daily thresholds.

To ensure that greater levels of development traffic do not use the local road network it is recommended that some Local Area Traffic Management (LATM) measures be implemented on Lansdowne Street, Highland Street and Kimberley Street to both deter vehicles from using and slow vehicles on these local roads. The details of any LATM measures would be developed, in consultation with Council and local residents, as part of the Development Application.

The location of the potential future LATM measures is illustrated in Figure 5.7.

Figure 5.7: Potential LATM Measures





#### 5.4.3 Summary

Against existing traffic volumes in the vicinity of the site, the additional traffic generated by the proposed development could not be expected to compromise the safety or function of the surrounding road network.

## 5.5 Staging

The development is proposed to be developed in three stages, as illustrated in Figure 5.8.



Figure 5.8: Indicative Staging Plan

A summary of the vehicle access arrangements for each stage are provided in Table 5.8.

| Table 5.8: | Vehicle | Access | Provisions  | by  | Stage |
|------------|---------|--------|-------------|-----|-------|
| Table 5.0. | Venicic | ACCC33 | 11041310113 | ~ 7 | Judge |

| Change            |                | Vehicle Access Provisions |                 |
|-------------------|----------------|---------------------------|-----------------|
| Stage             | Woodville Road | Lansdowne Street          | Highland Street |
| Stage 1           | √              | √                         | ×               |
| Stage 2           | $\checkmark$   | ✓                         | $\checkmark$    |
| Stage 3 (Overall) | √              | ✓                         | $\checkmark$    |

Table 5.8 indicates that initially vehicle access (Stage 1) will be provided from Woodville Road and Lansdowne Street.

As detailed in Table 5.3 the non-residential land uses are anticipated to generate the bulk of the traffic from the site. As such, there would be an opportunity to provide vehicle access to the

Stage 1 residential land uses via Lansdowne Road (and/or a temporary left-in, left-out Woodville Rod access) only prior to the development of the non-residential land uses. Following the development of the non-residential land uses the provision of the new signalised intersection to Woodville Road would be required to accommodate the additional traffic generation from the site.



# 6. Conclusion

Based on the analysis and discussions presented within this report, the following conclusions are made:

- i It is proposed to rezone the subject site from B6 Enterprise Corridor and R2 Low Density Residential to B4 Mixed Use Zone.
- ii It is recommended that car parking for the future land uses be provided in accordance with the requirements of the Parramatta DCP 2011. There may be an opportunity to share (part of) the residential visitor parking provision with the retail parking.
- iii It is recommended that bicycle parking for the future land uses be provided in accordance with the requirements of the Parramatta DCP 2011.
- iv It is proposed to provide a future active travel corridor along Lansdowne Street connecting the site to the Railway Terrace shared path and Merrylands Railway Station.
- The development is anticipated to generate in the order of 720 (including 580 new trips) and 870 (including 700 new trips) vehicle trips during the weekday PM and Saturday lunchtime peak hours, respectively.
- vi A new signalised intersection would be required at the existing Woodville Road/ Kimberley Street intersection, incorporating a new western approach servicing the subject site. Traffic modelling and initial sketch design indicates that such an intersection is feasible, however further design development and consultation with RMS would be required to progress the proposed traffic signals.
- vii There is adequate capacity in the surrounding road network, incorporating the proposed mitigating works, to cater for the traffic generated by the proposed development.
- viii The proposed traffic signals at the existing Woodville Road/ Kimberley Street intersection provide local access benefits through additional right turn opportunities to/from Woodville Road. The traffic signals would also provide a safe pedestrian crossing point along an otherwise difficult pedestrian corridor.
- ix A 'seagull' intersection treatment could be provided at the Oxford Street/ Highland Street intersection to improve operation during peak school pick-up and drop-off periods.
- x The development is anticipated to generate in the order of 7,300 daily vehicle movements, including 5,900 new vehicle trips and 1,400 passer by trips.
- xi The predicted future daily traffic volumes on Lansdowne Street and Highland Street are within their environmental capacities.
- xii It is recommended that LATM measures be implemented on Lansdowne Street, Highland Street and Kimberley Street to minimise development traffic using these residential streets. Such treatments should be cognisant of Granville South Public School operations and safety.
- xiii Against existing traffic volumes in the vicinity of the site, the additional traffic generated by the proposed development could not be expected to compromise the safety or function of the surrounding road network.
- xiv It is anticipated that the proposed development would be delivered in three stages. There would be an opportunity to deliver part of the residential component of the development prior to the implementation of the signalised intersection to Woodville Road.





Appendix A

Survey Results





| Intersectio   | on of Woodville   | Road and Kimberley Street | Saturday, 9 May 2015  |
|---|---|---------------------------|-----------------------|
|   |   |                           | Austraffic            |
| Survey Start<br>Intersection Type<br>Intersection No.<br>North Approach<br>East Approach<br>South Approach<br>West Approach | 10:00 AM<br>T Junction<br>1<br>Woodville Road<br>Kimberley Street<br>Woodville Road |                           | Woodville Road        |
| Date  | 9/05/15   |                           |                       |
| Classification  | Light Heavy   | SILSISIIIIASI             | 8 7<br>Woodville Road |

VEHICLE MOVEMENT TIME PERIOD 2 4 6 8 3 Light Heavy  $\Sigma$  
 Light
 Heavy
 £
 Light</t Light Heavy 10:00 10:15 10:30 10:45 11:00 11.15 11:30 11:45 12:00 12:15 12:30 12:45

|         |       |         |       |      |       |       |       |    |       | VEF   | ICLE I | MOVE  | MENT |    |       |       |    |       |      |      |       |      |      |
|---------|-------|---------|-------|------|-------|-------|-------|----|-------|-------|--------|-------|------|----|-------|-------|----|-------|------|------|-------|------|------|
| TIME PI | ERIOD |         | 2     |      |       | 3     |       |    |       | 4     |        |       | 6    |    |       | 7     |    |       | 8    |      | GRA   | ND T | OTAL |
|         |       | Light I | leavy | Σ    | Light | t Hea | vy    | Σ  | Light | Heavy | Σ      | Light | Heav | yΣ | Light | Heavy | (Σ | Light | Heav | yΣ   | Light | Heav | yΣ   |
| 10:00 - | 11:00 | 1158    | 50    | 1208 | 8     | : 0   |       | 8  | 0     | 0     | 0      | 61    | 1    | 62 | 0     | 0     | 0  | 1352  | 59   | 1411 | 2579  | 110  | 2689 |
| 10:15 - | 11:15 | 1247    | 52    | 1299 | 9     | 0     | 1.1   | 9  | 0     | 0     | 0      | 67    | 2    | 69 | 0     | 0     | 0  | 1299  | 58   | 1357 | 2622  | 112  | 2734 |
| 10:30 - | 11:30 | 1285    | 54    | 1339 | 8     | 0     | i.    | 8  | 0     | 0     | 0      | 64    | 2    | 66 | 0     | 0     | 0  | 1322  | 57   | 1379 | 2679  | 113  | 2792 |
| 10:45 - | 11:45 | 1332    | 65    | 1397 | 8     | 0     | ě.    | 8  | 0     | 0     | 0      | 69    | 2    | 71 | 0     | 0     | 0  | 1381  | 55   | 1436 | 2790  | 122  | 2912 |
| 11:00 - | 12:00 | 1373    | 60    | 1433 | 10    | 1     | : 1   | 11 | 0     | 0     | 0      | 64    | 2    | 66 | 0     | 0     | 0  | 1386  | 58   | 1444 | 2833  | 121  | 2954 |
| 11:15 - | 12:15 | 1395    | 62    | 1457 | 10    | 1     | 1     | 11 | 0     | 0     | 0      | 56    | 1    | 57 | 1     | 0     | 1  | 1421  | 60   | 1481 | 2883  | 124  | 3007 |
| 11:30 - | 12:30 | 1458    | 65    | 1523 | 8     | 1     |       | 9  | 0     | 0     | 0      | 56    | 0    | 56 | 1     | 0     | 1  | 1416  | 59   | 1475 | 2939  | 125  | 3064 |
| 11:45 - | 12:45 | 1466    | 62    | 1528 | 8     | 2     | - 1 1 | 10 | 0     | 0     | 0      | 59    | 0    | 59 | 1     | 0     | 1  | 1413  | 64   | 1477 | 2947  | 128  | 3075 |
| 12:00 - | 13:00 | 1486    | 61    | 1547 | 7     | 1     |       | 8  | 0     | 0     | 0      | 58    | 0    | 58 | 1     | 0     | 1  | 1419  | 58   | 1477 | 2971  | 120  | 3091 |

Camera Position



|               |                      |                      | VEHICLE I            | MOVEMENT             |                      |                      |                      |                      | VEHICLE N            | NOVEMENT                                  |                      |                      |
|---------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|---|----------------------|----------------------|
| TIME PERIOD   | 1                    | 2                    | 3                    | 4                    | 5                    | 6                    | 7                    | 8                    | 9                    | 10 11                                     | 12                   | GRAND TOTAL          |
|               | Light Heavy $\Sigma$ Light Heavy $\Sigma$ | Light Heavy $\Sigma$ | Light Heavy $\Sigma$ |
| 10:00 - 10:15 | 9 0 9                | 258 15 273           | 2 0 2                | 0 0 0                | 0 0 0                | 4 0 4                | 0 0 0                | 356 15 371           | 1 0 1                | 1 0 1 1 0 1                               | 6 0 6                | 638 30 668           |
| 10:15 - 10:30 | 13 0 13              | 282 14 296           | 6 0 6                | 0 0 0                | 0 0 0                | 5 0 5                | 1 0 1                | 317 13 330           | 3 0 3                | 4 0 4 0 0 0                               | 5 0 5                | 636 27 663           |
| 10:30 - 10:45 |                      | 307 6 313            | 4 0 4                | 0 0 0                | 0 0 0                | 6 0 6                | 0 0 0                | 322 16 338           | 10 0 10              | 1 0 1 4 0 4                               | 9 0 9                | 676 23 699           |
| 10:45 - 11:00 | 9 0 9                | 292 15 307           | 6 0 6                | 0 0 0                | 0 0 0                | 7 0 7                | 0 0 0                | 333 16 349           | 3 0 3                | 1 0 1 3 0 3                               | 10 0 10              | 664 31 695           |
| 11:00 - 11:15 | 12 0 12              | 343 15 358           | 4 1 5                | 0 0 0                | 0 0 0                | 8 1 9                | 0 0 0                | 306 13 319           | 9 0 9                | 2 1 3 2 0 2                               | 8 0 8                | 694 31 725           |
| 11:15 - 11:30 | 15 1 16              | 310 15 325           | 4 0 4                | 0 0 0                | 0 0 0                | 6 0 6                | 0 0 0                | 336 13 349           | 4 0 4                | 2 0 2 4 0 4                               | 12 1 13              | 693 30 723           |
| 11:30 - 11:45 | i 19 0 19            | 351 18 369           | 3 0 3                | 0 0 0                | 0 0 0                | 6 0 6                | 0 0 0                | 391 12 403           | 9 1 10               | 3 0 3 3 0 3                               | 14 0 14              | 799 31 830           |
| 11:45 - 12:00 | 9 0 9                | 333 11 344           | 4 0 4                | 0 0 0                | 0 0 0                | 7 0 7                | 0 0 0                | 353 19 372           | 7 0 7                | 2 0 2 1 0 1                               | 8 0 8                | 724 30 754           |
| 12:00 - 12:15 | i 13 1 14            | 361 20 381           | 2 0 2                | 1 0 1                | 0 0 0                | 3 0 3                | 0 0 0                | 328 15 343           | 9 0 9                | 7 0 7 0 0 0                               | 7 0 7                | 731 36 767           |
| 12:15 - 12:30 | 13 0 13              | 377 17 394           | 5 0 5                | 0 0 0                | 0 0 0                | 10 0 10              | 0 0 0                | 312 11 323           | 7 0 7                | 2 0 2 2 0 2                               | 6 0 6                | 734 28 762           |
| 12:30 - 12:45 | 20 2 22              | 367 16 383           | 3 0 3                | 0 0 0                | 0 0 0                | 7 0 7                | 0 0 0                | 397 19 416           | 6 0 6                | 0 0 0 3 0 3                               | 11 0 11              | 814 37 851           |
| 12:45 - 13:00 | 16 0 16              | 350 10 360           | 4 0 4                | 0 0 0                | 0 0 0                | 4 0 4                | 0 0 0                | 352 13 365           | 10 0 10              | 5 0 5 2 0 2                               | 11 0 11              | 754 23 777           |
| Σ             | 161 5 166            | 3931 172 4103        | 47 1 48              | 1 0 1                | 0 0 0                | 73 1 74              | 1 0 1                | 4103 175 4278        | 78 1 79              | 30 1 31 25 0 25                           | 107 1 108            | 8557 357 8914        |

| HOURLY FLOW   |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |
|---------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|
|               |                      |                      | VEHICLE I            | MOVEMENT             |                      |                      |                      |                      | V                    | EHICLE MOVEMEN       | Т                    |                      |                      |
| TIME PERIOD   | 1                    | 2                    | 3                    | 4                    | 5                    | 6                    | 7                    | 8                    | 9                    | 10                   | 11                   | 12                   | GRAND TOTAL          |
|               | Light Heavy $\Sigma$ |
| 10:00 - 11:00 | 44 1 45              | 1139 50 1189         | 18 0 18              | 0 0 0                | 0 0 0                | 22 0 22              | 1 0 1                | 1328 60 1388         | 3 17 0 17            | 7 0 7                | 8 0 8                | 30 0 30              | 2614 111 2725        |
| 10:15 - 11:15 | 47 1 48              | 1224 50 1274         | 20 1 21              | 0 0 0                | 0 0 0                | 26 1 27              | 1 0 1                | 1278 58 1336         | 6 25 0 25            | 8 1 9                | 9 0 9                | 32 0 32              | 2670 112 2782        |
| 10:30 - 11:30 | 49 2 51              | 1252 51 1303         | 18 1 19              | 0 0 0                | 0 0 0                | 27 1 28              | 0 0 0                | 1297 58 1355         | 5 26 0 26            | 6 1 7                | 13 0 13              | 39 1 40              | 2727 115 2842        |
| 10:45 - 11:45 | 55 1 56              | 1296 63 1359         | 17 1 18              | 0 0 0                | 0 0 0                | 27 1 28              | 0 0 0                | 1366 54 1420         | 25 1 26              | 8 1 9                | 12 0 12              | 44 1 45              | 2850 123 2973        |
| 11:00 - 12:00 | 55 1 56              | 1337 59 1396         | 15 1 16              | 0 0 0                | 0 0 0                | 27 1 28              | 0 0 0                | 1386 57 1443         | 3 29 1 30            | 9 : 1 : 10           | 10 0 10              | 42 1 43              | 2910 122 3032        |
| 11:15 - 12:15 | 56 2 58              | 1355 64 1419         | 13 0 13              | 1 0 1                | 0 0 0                | 22 0 22              | 0 0 0                | 1408 59 1467         | 29 1 30              | 14 0 14              | 8 0 8                | 41 1 42              | 2947 127 3074        |
| 11:30 - 12:30 | 54 1 55              | 1422 66 1488         | 14 0 14              | 1 0 1                | 0 0 0                | 26 0 26              | 0 0 0                | 1384 57 1441         | 32 1 33              | 14 0 14              | 6 0 6                | 35 0 35              | 2988 125 3113        |
| 11:45 - 12:45 | 55 3 58              | 1438 64 1502         | 14 0 14              | 1 0 1                | 0 0 0                | 27 0 27              | 0 0 0                | 1390 64 1454         | 29 0 29              | 11 0 11              | 6 0 6                | 32 0 32              | 3003 131 3134        |
| 12:00 - 13:00 | 62 3 65              | 1455 63 1518         | 14 0 14              | 1 0 1                | 0 0 0                | 24 0 24              | 0 0 0                | 1389 58 1447         | 32 0 32              | 14 0 14              | 7 0 7                | 35 0 35              | 3033 124 3157 F      |

| Intersectio   | on of Woodville Roa  | d and Kimberley Street | Wednesday, 13 May 2015 |
|---|--|------------------------|------------------------|
|   |  |                        | Austraffic             |
| Survey Start<br>Intersection Type<br>Intersection No.<br>North Approach<br>East Approach<br>South Approach<br>West Approach | 7:00 AM 16:00 PM<br>T Junction<br>Woodville Road<br>Kimberley Street<br>Woodville Road |                        | Woodville Road         |
| Date  | 13/05/15   |                        |                        |
| Classification  | Light Heavy  | 2 C REFERENCE          | 8 7<br>Woodville Road  |

Camera Position

|      |        |      |       |       |      |       |       |    |       | VEF   | ICLE I | MOVEN | IENT  |    |       |       |   |       |       |      |       |       |      |
|------|--------|------|-------|-------|------|-------|-------|----|-------|-------|--------|-------|-------|----|-------|-------|---|-------|-------|------|-------|-------|------|
| TIM  | IE PER | IOD  |       | 2     |      |       | 3     |    |       | 4     |        |       | 6     |    |       | 7     |   |       | 8     |      | GRA   | ND TO | DTAL |
|      |        |      | Light | Heavy | Σ    | Light | Heavy | Σ  | Light | Heavy | Σ      | Light | Heavy | Σ  | Light | Heavy | Σ | Light | Heavy | Σ    | Light | Heavy | Σ    |
| 7:00 | -      | 7:15 | 284   | 30    | 314  | 1     | 0     | 1  | 0     | 0     | 0      | 5     | 1     | 6  | 0     | 0     | 0 | 437   | 39    | 476  | 727   | 70    | 797  |
| 7:15 | -      | 7:30 | 280   | 24    | 304  | 0     | 0     | 0  | 0     | 0     | 0      | 11    | 0     | 11 | 0     | 0     | 0 | 455   | 41    | 496  | 746   | 65    | 811  |
| 7:30 | -      | 7:45 | 301   | 22    | 323  | 0     | 0     | 0  | 0     | 0     | 0      | 6     | 1     | 7  | 0     | 0     | 0 | 369   | 27    | 396  | 676   | 50    | 726  |
| 7:45 | -      | 8:00 | 302   | 26    | 328  | 1     | 0     | 1  | 0     | 0     | 0      | 4     | 2     | 6  | 0     | 0     | 0 | 336   | 23    | 359  | 643   | 51    | 694  |
| 8:00 | -      | 8:15 | 281   | 19    | 300  | 5     | 1     | 6  | 0     | 0     | 0      | 9     | 0     | 9  | 1     | 0     | 1 | 289   | 18    | 307  | 585   | 38    | 623  |
| 8:15 | -      | 8:30 | 260   | 26    | 286  | 2     | 0     | 2  | 0     | 0     | 0      | 6     | 1     | 7  | 0     | 0     | 0 | 282   | 30    | 312  | 550   | 57    | 607  |
| 8:30 | -      | 8:45 | 295   | 26    | 321  | 1     | 0     | 1  | 0     | 0     | 0      | 10    | 0     | 10 | 0     | 0     | 0 | 230   | 24    | 254  | 536   | 50    | 586  |
| 8:45 | -      | 9:00 | 291   | 27    | 318  | 8     | 0     | 8  | 0     | 0     | 0      | 7     | 2     | 9  | 0     | 0     | 0 | 196   | 28    | 224  | 502   | 57    | 559  |
|      | Σ      |      | 2294  | 200   | 2494 | 18    | 1     | 19 | 0     | 0     | 0      | 58    | 7     | 65 | 1     | 0     | 1 | 2594  | 230   | 2824 | 4965  | 438   | 5403 |

|       |       |       |       |       |      |       |       |    |       | VEF   | ICLE N | NOVEN | IENT  |     |       |       |   |       |       |      |       |       |      |
|-------|-------|-------|-------|-------|------|-------|-------|----|-------|-------|--------|-------|-------|-----|-------|-------|---|-------|-------|------|-------|-------|------|
| TIME  | E PEF | RIOD  |       | 2     |      |       | 3     |    |       | 4     |        |       | 6     |     |       | 7     |   |       | 8     |      | GRA   | ND TO | DTAL |
|       |       |       | Light | Heavy | Σ    | Light | Heavy | Σ  | Light | Heavy | Σ      | Light | Heavy | Σ   | Light | Heavy | Σ | Light | Heavy | Σ    | Light | Heavy | Σ    |
| 16:00 | -     | 16:15 | 456   | 23    | 479  | 2     | 0     | 2  | 0     | 0     | 0      | 23    | 1     | 24  | 0     | 0     | 0 | 348   | 24    | 372  | 829   | 48    | 877  |
| 16:15 | -     | 16:30 | 453   | 33    | 486  | 2     | 0     | 2  | 0     | 0     | 0      | 20    | 0     | 20  | 0     | 0     | 0 | 356   | 21    | 377  | 831   | 54    | 885  |
| 16:30 | -     | 16:45 | 438   | 16    | 454  | 1     | 0     | 1  | 0     | 0     | 0      | 15    | 1     | 16  | 0     | 0     | 0 | 312   | 16    | 328  | 766   | 33    | 799  |
| 16:45 | -     | 17:00 | 419   | 23    | 442  | 4     | 0     | 4  | 0     | 0     | 0      | 17    | 0     | 17  | 0     | 0     | 0 | 346   | 27    | 373  | 786   | 50    | 836  |
| 17:00 | -     | 17:15 | 430   | 16    | 446  | 3     | 0     | 3  | 0     | 0     | 0      | 23    | 4     | 27  | 0     | 0     | 0 | 348   | 21    | 369  | 804   | 41    | 845  |
| 17:15 | -     | 17:30 | 443   | 14    | 457  | 4     | 0     | 4  | 0     | 0     | 0      | 13    | 0     | 13  | 0     | 0     | 0 | 411   | 19    | 430  | 871   | 33    | 904  |
| 17:30 | -     | 17:45 | 437   | 18    | 455  | 5     | 0     | 5  | 0     | 0     | 0      | 25    | 0     | 25  | 0     | 0     | 0 | 330   | 9     | 339  | 797   | 27    | 824  |
| 17:45 | -     | 18:00 | 431   | 20    | 451  | 2     | 0     | 2  | 0     | 0     | 0      | 22    | 0     | 22  | 0     | 0     | 0 | 387   | 15    | 402  | 842   | 35    | 877  |
|       | Σ     |       | 3507  | 163   | 3670 | 23    | 0     | 23 | 0     | 0     | 0      | 158   | 6     | 164 | 0     | 0     | 0 | 2838  | 152   | 2990 | 6526  | 321   | 6847 |

| HOURLY FLOW                |               |               |               |               |                      |                      |                      |
|----------------------------|---------------|---------------|---------------|---------------|----------------------|----------------------|----------------------|
|                            |               |               | VEHICLE I     | MOVEMENT      |                      |                      |                      |
| TIME PERIOD                | 2             | 3             | 4             | 6             | 7                    | 8                    | GRAND TOTAL          |
|                            | Light Heavy S | Light Heavy S | Light Heavy S | Light Heavy S | Light Heavy $\Sigma$ | Light Heavy $\Sigma$ | Light Heavy $\Sigma$ |
| 7:00 - 8:00<br>7:15 - 8:15 | 1167 102 1269 | 2 0 2         | 0 0 0         | 26 4 30       | 0 0 0                | 1597 130 1727        | 2792 236 3028 F      |
| 7:15 - 8:15                | 1164 91 1255  | 6 1 7         | 0 0 0         | 30 3 33       | 1 0 1                | 1449 109 1558        | 2650 204 2854        |
| 7:30 - 8:30                | 1144 93 1237  | 8 1 9         | 0 0 0         | 25 4 29       | 1 0 1                | 1276 98 1374         | 2454 196 2650        |
| 7:45 - 8:45                | 1138 97 1235  | 9 1 10        | 0 0 0         | 29 3 32       | 1 0 1                | 1137 95 1232         | 2314 196 2510        |
| 8:00 - 9:00                | 1127 98 1225  | 16 1 17       | 0 0 0         | 32 3 35       | 1 0 1                | 997 100 1097         | 2173 202 2375        |

#### HOURLY FLOW

|       |       |       |       |       |      |       |      |     |    |       |    | VEH | ICLE | MOVE  | MEN. | Г   |    |      |      |      |   |      |      |     |      |       |      |                  |
|-------|-------|-------|-------|-------|------|-------|------|-----|----|-------|----|-----|------|-------|------|-----|----|------|------|------|---|------|------|-----|------|-------|------|------------------|
| TIME  | E PEF | RIOD  |       | 2     |      |       | 3    | 3   |    |       | 4  | 4   |      |       | 6    | 6   |    |      |      | 7    |   |      | 8    | 3   |      | GRA   | ND . | TOTAL            |
|       |       |       | Light | Heavy | Σ    | Light | t He | avy | Σ  | Light | He | avy | Σ    | Light | t He | avy | Σ  | Ligh | t He | eavy | Σ | Ligh | t He | avy | Σ    | Light | Heav | vy Σ             |
| 16:00 | -     | 17:00 | 1766  | 95    | 1861 | 9     | (    | )   | 9  | 0     |    | )   | 0    | 75    | 1    | 2   | 77 | 0    |      | 0    | 0 | 136  | 2:8  | 8   | 1450 | 3212  | 185  | 5 3397           |
| 16:15 | -     | 17:15 | 1740  | 88    | 1828 | 10    | (    | )   | 10 | 0     | 1  | )   | 0    | 75    | 1    | 5   | 80 | 0    |      | 0    | 0 | 136  | 2 8  | 5   | 1447 | 3187  | 178  | 3 3365<br>7 3384 |
| 16:30 | -     | 17:30 | 1730  | 69    | 1799 | 12    | . (  | )   | 12 | 0     | 1  | )   | 0    | 68    | . (  | 5   | 73 | 0    | 1    | 0    | 0 | 141  | 7 8  | 3   | 1500 | 3227  | 157  | 7 3384           |
| 16:45 | -     | 17:45 | 1729  | 71    | 1800 | 16    | . (  | )   | 16 | 0     | 1  | )   | 0    | 78    | 4    |     | 82 | 0    | 1    | 0    | 0 | 143  | 5 7  | 6   | 1511 | 3258  | 151  | 1 3409           |
| 17:00 | -     | 18:00 |       |       | 1809 | 14    | (    | )   | 14 | 0     | 1  | 0   | 0    | 83    | 4    |     | 87 | 0    | 1    | 0    | 0 | 147  | 6 6  | 4   | 1540 | 3314  | 136  | 3450             |

| Intersectio   | on of Woodville Roa   | d, Lansdowne Street and Earl Street | Wednesday, 13 May 2015                                      |
|---|---|-------------------------------------|---|
|   |   |                                     | Austraffic  |
| Survey Start<br>Intersection Type<br>Intersection No.<br>North Approach<br>East Approach<br>South Approach<br>West Approach | 7:00 AM 16:00 PM<br>Cross Junction<br>Woodville Road<br>Earl Street<br>Woodville Road<br>Lansdowne Street | Line Sites                          | Woodville Road<br>N<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 |
| Date  | 13/05/15  | ransde                              | ·····································                       |
| Classification  | Light Heavy   | 2012-05-0107-05-02                  | 9 7<br>8<br>Woodville Road                                  |

| Camera Position |             |    |         |       |      |       |       |         |       |       |     |      |        |       |       |         |       |    |       |       |    |       |       |      |       |       |         |       |       |    |       |      |    |       |       |     |       |       |      |
|-----------------|-------------|----|---------|-------|------|-------|-------|---------|-------|-------|-----|------|--------|-------|-------|---------|-------|----|-------|-------|----|-------|-------|------|-------|-------|---------|-------|-------|----|-------|------|----|-------|-------|-----|-------|-------|------|
|                 |             |    |         |       |      |       | VE    | HICLE I | MOVE  | MENT  |     |      |        |       |       |         |       |    |       |       |    |       |       |      |       | VE    | HICLE I | MOVEN | IENT  |    |       |      |    |       |       |     |       |       |      |
| TIME PERIOD     | 1           |    |         | 2     |      |       | 3     |         |       | 4     |     |      | 5      | ;     |       |         | 6     |    |       | 7     |    |       | 8     |      |       | 9     |         |       | 10    |    |       | 11   |    |       | 12    |     | GRA   | ND TO | TAL  |
|                 | Light Heavy | Σ  | Light I | leavy | Σ    | Light | Heavy | Σ       | Light | Heavy | / Σ | Ligh | it Hea | avy Σ | E   I | Light H | leavy | Σ  | Light | Heavy | Σ  | Light | Heavy | γ Σ  | Light | Heavy | Σ       | Light | Heavy | Σ  | Light | Heav | yΣ | Light | Heavy | ί Σ | Light | Heavy | Σ    |
| 7:00 - 7:15     | 8 1         | 9  | 282     | 30    | 312  | 2     | 0     | 2       | 0     | 0     | 0   | 0    | 0      | (     | )     | 3       | 0     | 3  | 0     | 0     | 0  | 437   | 38    | 475  | 2     | 0     | 2       | 0     | 0     | 0  | 0     | 0    | 0  | 8     | 0     | 8   | 742   | 69    | 811  |
| 7:15 - 7:30     | 8 0         | 8  | 269     | 24    | 293  | 0     | 0     | 0       | 0     | 0     | 0   | 0    | C      | ) (   | וו    | 7       | 0     | 7  | 0     | 0     | 0  | 456   | 41    | 497  | 1     | 0     | 1       | 2     | 0     | 2  | 0     | 0    | 0  | 6     | 0     | 6   | 749   | 65    | 814  |
| 7:30 - 7:45     | 6 1         | 7  | 291     | 23    | 314  | 4     | 0     | 4       | 0     | 0     | 0   | 0    | C      | ) (   | וו    | 7       | 0     | 7  | 3     | 0     | 3  | 357   | 27    | 384  | 9     | 0     | 9       | 3     | 0     | 3  | 5     | 0    | 5  | 3     | 1     | 4   | 688   | 52    | 740  |
| 7:45 - 8:00     | 7 0         | 7  | 298     | 25    | 323  | 2     | 0     | 2       | 0     | 0     | 0   | 0    | 0      | ) (   | )     | 2       | 0     | 2  | 19    | 0     | 19 | 287   | 22    | 309  | 20    | 0     | 20      | 2     | 0     | 2  | 3     | 0    | 3  | 4     | 0     | 4   | 644   | 47    | 691  |
| 8:00 - 8:15     | 11 0        | 11 | 288     | 18    | 306  | 0     | 0     | 0       | 0     | 0     | 0   | 0    | 0      | ) (   | )     | 5       | 2     | 7  | 17    | 2     | 19 | 265   | 15    | 280  |       | 1     | 10      | 2     | 0     | 2  | 6     | 0    | 6  | 7     | 0     | 7   | 610   | 38    | 648  |
| 8:15 - 8:30     | 10 0        | 10 | 252     | 26    | 278  | 2     | 1     | 3       | 0     | 0     | 0   | 0    | : C    | ) (   | )     | 6       | 0     | 6  | 11    | 1     | 12 | 276   | 30    | 306  | 4     | 0     | 4       | 5     | 0     | 5  | 6     | 0    | 6  | 10    | 0     | 10  | 582   | 58    | 640  |
| 8:30 - 8:45     | 14 0        | 14 | 285     | 26    | 311  | 2     | 0     | 2       | 0     | 0     | 0   | 0    | 0      | ) (   | )     | 14      | 0     | 14 | 9     | 0     | 9  | 209   | 22    | 231  | 4     | 1     | 5       | 2     | 0     | 2  | 4     | 1    | 5  | 3     | 0     | 3   | 546   | 50    | 596  |
| 8:45 - 9:00     | 16 0        | 16 | 282     | 26    | 308  | 5     | 1     | 6       | 0     | 0     | 0   | 0    | C      | ) (   | )     | 15      | 0     | 15 | 14    | 0     | 14 | 194   | 29    | 223  | 6     | 0     | 6       | 1     | 0     | 1  | 3     | 0    | 3  | 8     | 0     | 8   | 544   | 56    | 600  |
| Σ               | 80 2        | 82 | 2247    | 198   | 2445 | 17    | 2     | 19      | 0     | 0     | 0   | 0    | C      | ) (   | )     | 59      | 2     | 61 | 73    | 3     | 76 | 2481  | 224   | 2705 | 55    | 2     | 57      | 17    | 0     | 17 | 27    | 1    | 28 | 49    | 1     | 50  | 5105  | 435   | 5540 |

Woodville Road

|               |                      |                      | VEHICLE N            | NOVEMENT             |                      |                      |                      |                      |                      | VEHICLE MOVEMENT     | Г                    |                      |                      |
|---------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|
| TIME PERIOD   | 1                    | 2                    | 3                    | 4                    | 5                    | 6                    | 7                    | 8                    | 9                    | 10                   | 11                   | 12                   | GRAND TOTAL          |
|               | Light Heavy $\Sigma$ |
| 16:00 - 16:15 | 29 1 30              | 431 25 456           | 10 0 10              | 0 0 0                | 0 0 0                | 13 0 13              | 0 0 0                | 345 24 369           | 11 0 11              | 2 0 2                | 5 1 6                | 6 0 6                | 852 51 903           |
| 16:15 - 16:30 | 18 0 18              | 443 31 474           | 7 0 7                | 0 0 0                | 1 0 1                | 12 0 12              | 0 0 0                | 351 21 372           | 4 0 4                | 2 0 2                | 2 0 2                | 7 0 7                | 847 52 899           |
| 16:30 - 16:45 | 23 0 23              | 421 16 437           | 8 1 9                | 0 0 0                | 0 0 0                | 9 0 9                | 0 0 0                | 304 16 320           | 9 0 9                | 2 0 2                | 1 0 1                | 8 0 8                | 785 33 818           |
| 16:45 - 17:00 | 23 2 25              | 425 24 449           | 9 0 9                | 0 0 0                | 0 0 0                | 12 0 12              | 1 0 1                | 340 25 365           | 5 0 5                | 3 0 3                | 0 0 0                | 10 0 10              | 828 51 879           |
| 17:00 - 17:15 | 22 2 24              | 393 14 407           | 4 0 4                | 0 0 0                | 0 0 0                | 18 1 19              | 0 0 0                | 349 22 371           | 8 1 9                | 3 0 3                | 2 0 2                | 5 1 6                | 804 41 845           |
| 17:15 - 17:30 | 20 0 20              | 433 14 447           | 3 1 4                | 0 0 0                | 0 0 0                | 11 0 11              | 0 0 0                | 404 18 422           | 6 1 7                | 2 0 2                | 2 0 2                | 7 0 7                | 888 34 922           |
| 17:30 - 17:45 | 29 0 29              | 422 18 440           | 3 0 3                | 0 0 0                | 0 0 0                | 13 0 13              | 0 0 0                | 329 9 338            | 10 0 10              | 2 0 2                | 1 0 1                | 14 0 14              | 823 27 850           |
| 17:45 - 18:00 | 22 0 22              | 421 20 441           | 9 0 9                | 0 0 0                | 0 0 0                | 12 0 12              | 0 0 0                | 380 15 395           | 4 0 4                | 2 0 2                | 2 0 2                | 6 0 6                | 858 35 893           |
| Σ             | 186 5 191            | 3389 162 3551        | 53 2 55              | 0 0 0                | 1 0 1                | 100 1 101            | 1 0 1                | 2802 150 2952        | 57 2 59              | 18 0 18              | 15 1 16              | 63 1 64              | 6685 324 7009        |

| HOURLY FLOW |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |  |
|-------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|--|
|             |                      |                      | VEHICLE              | MOVEMENT             |                      |                      |                      |                      |                      | VEHICLE MOVEMEN      | Т                    |                      |                      |  |
| TIME PERIOD | 1                    | 2                    | 3                    | 4                    | 5                    | 6                    | 7                    | 8                    | 9                    | 10                   | 11                   | 12                   | GRAND TOTAL          |  |
|             | Light Heavy $\Sigma$ |  |
| 7:00 - 8:00 | 29 2 31              | 1140 102 1242        | 8 0 8                | 0 0 0                | 0 0 0                | 19 0 19              | 22 0 22              | 1537 128 1665        | 32 0 32              | 7 0 7                | 8 0 8                | 21 1 22              | 2823 233 3056 F      |  |
| 7:15 - 8:15 | 32 1 33              | 1146 90 1236         | 6 0 6                | 0 0 0                | 0 0 0                | 21 2 23              | 39 : 2 : 41          | 1365 105 1470        | 39 1 40              | 9 0 9                | 14 : 0 : 14          | 20 1 21              | 2691 : 202 : 2893    |  |
| 7:30 - 8:30 | 34 1 35              | 1129 92 1221         | 8 1 9                | 0 0 0                | 0 0 0                | 20 2 22              | 50 3 53              | 1185 94 1279         | 42 1 43              | 12 0 12              | 20 0 20              | 24 1 25              | 2524 195 2719        |  |
| 7:45 - 8:45 | 42 0 42              | 1123 95 1218         | 6 1 7                | 0 0 0                | 0 0 0                | 27 2 29              | 56 3 59              | 1037 89 1126         | 37 2 39              | 11 0 11              | 19 1 20              | 24 0 24              | 2382 193 2575        |  |
| 8:00 - 9:00 | 51 0 51              | 1107 96 1203         | 9 2 11               | 0 0 0                | 0 0 0                | 40 2 42              | 51 3 54              | 944 96 1040          | 23 2 25              | 10 0 10              | 19 1 20              | 28 0 28              | 2282 202 2484        |  |

| HOURLY FLOW   |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |                      |
|---------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|
|               |                      |                      | VEHICLE              | MOVEMENT             |                      |                      |                      |                      |                      | VEHICLE MOVEMEN      | Т                    |                      |                      |
| TIME PERIOD   | 1                    | 2                    | 3                    | 4                    | 5                    | 6                    | 7                    | 8                    | 9                    | 10                   | 11                   | 12                   | GRAND TOTAL          |
|               | Light Heavy $\Sigma$ |
| 16:00 - 17:00 | 93 3 96              | 1720 96 1816         | 34 1 35              | 0 0 0                | 1 0 1                | 46 0 46              | 1 0 1                | 1340 86 1426         | 29 0 29              | 9 0 9                | 8 1 9                | 31 0 31              | 3312 187 3499        |
| 16:15 - 17:15 | 86 4 90              | 1682 85 1767         | 28 1 29              | 0 0 0                | 1 0 1                | 51 1 52              | 1 0 1                | 1344 84 1428         | 26 1 27              | 10 0 10              | 5 0 5                | 30 1 31              | 3264 177 3441        |
| 16:30 - 17:30 | 88 4 92              | 1672 68 1740         | 24 2 26              | 0 0 0                | 0 0 0                | 50 1 51              | 1 0 1                | 1397 81 1478         | 28 2 30              | 10 0 10              | 5 0 5                | 30 1 31              | 3305 159 3464        |
| 16:45 - 17:45 | 94 4 98              | 1673 70 1743         | 19 1 20              | 0 0 0                | 0 0 0                | 54 1 55              | 1 0 1                | 1422 74 1496         | 29 2 31              | 10 0 10              | 5 0 5                | 36 1 37              | 3343 153 3496        |
| 17:00 - 18:00 | 93 2 95              | 1669 66 1735         | 19 1 20              | 0 0 0                | 0 0 0                | 54 1 55              | 0 0 0                | 1462 64 1526         | 28 2 30              | 9 0 9                | 7 0 7                | 32 1 33              | 3373 137 3510 P      |

#### R.O.A.R. DATA Reliable, Original & Authentic Results

Ph.88196847, Fax 88196849, Mob.0418-239019

| All Vehicles | NO       | RTH      | WE   | ST       | SO    | UTH      |       |
|--------------|----------|----------|------|----------|-------|----------|-------|
|              | Wood     | /ille Rd | Oxfo | rd St    | Woodv | ville Rd |       |
| Time Per     | <u>R</u> | <u>T</u> | L    | <u>R</u> | L     | <u>T</u> | TOTAL |
| 0700 - 0715  | 24       | 247      | 25   | 142      | 61    | 457      | 956   |
| 0715 - 0730  | 47       | 295      | 40   | 168      | 52    | 450      | 1052  |
| 0730 - 0745  | 47       | 271      | 30   | 163      | 47    | 490      | 1048  |
| 0745 - 0800  | 34       | 295      | 25   | 196      | 97    | 521      | 1168  |
| 0800 - 0815  | 59       | 303      | 27   | 201      | 76    | 386      | 1052  |
| 0815 - 0830  | 51       | 302      | 27   | 190      | 62    | 440      | 1072  |
| 0830 - 0845  | 45       | 318      | 39   | 177      | 79    | 486      | 1144  |
| 0845 - 0900  | 68       | 260      | 25   | 131      | 79    | 370      | 933   |
| Period End   | 375      | 2291     | 238  | 1368     | 553   | 3600     | 8425  |

|             | NO           | NORTH |      | ST       | SO    | JTH      |       |
|-------------|--------------|-------|------|----------|-------|----------|-------|
|             | Woodville Rd |       | Oxfo | rd St    | Woodv | ville Rd |       |
| Peak Per    | <u>R</u>     | Ţ     | L    | <u>R</u> | L     | <u>T</u> | TOTAL |
| 0700 - 0800 | 152          | 1108  | 120  | 669      | 257   | 1918     | 4224  |
| 0715 - 0815 | 187          | 1164  | 122  | 728      | 272   | 1847     | 4320  |
| 0730 - 0830 | 191          | 1171  | 109  | 750      | 282   | 1837     | 4340  |
| 0745 - 0845 | 189          | 1218  | 118  | 764      | 314   | 1833     | 4436  |
| 0800 - 0900 | 223          | 1183  | 118  | 699      | 296   | 1682     | 4201  |



| Client       |          | : GTA     | Consul     | tants    |        |          |       |
|--------------|----------|-----------|------------|----------|--------|----------|-------|
| Job No/Na    | ame      | : 5621    | GUILD      | FORD     | Oxford | St       |       |
| Day/Dat      | te       | : Thurs   | sday / 2   | 1st Ma   | y 2015 |          |       |
| All Vehicles | NO       | RTH       | WE         | ST       | SO     | UTH      |       |
|              | Wood     | ville Rd  | Oxfo       | rd St    | Woodv  | ville Rd |       |
| Time Per     | <u>R</u> | T         | Ŀ          | <u>R</u> | Ŀ      | I        | TOTAL |
| 1430 - 1445  | 62       | 302       | 29         | 137      | 99     | 279      | 908   |
| 1445 - 1500  | 81       | 329       | 35         | 118      | 91     | 303      | 957   |
| 1500 - 1515  | 74       | 358       | 24         | 174      | 102    | 369      | 1101  |
| 1515 - 1530  | 63       | 408       | 25         | 134      | 110    | 369      | 1109  |
| 1530 - 1545  | 83       | 352       | 25         | 163      | 102    | 325      | 1050  |
| 1545 - 1600  | 127      | 399       | 21         | 130      | 120    | 361      | 1158  |
| 1600 - 1615  | 95       | 388       | 25         | 132      | 124    | 380      | 1144  |
| 1615 - 1630  | 104      | 417       | 22         | 151      | 145    | 346      | 1185  |
| 1630 - 1645  | 83       | 385       | 28         | 148      | 140    | 338      | 1122  |
| 1645 - 1700  | 104      | 401       | 23         | 151      | 137    | 309      | 1125  |
| 1700 - 1715  | 111      | 366       | 25         | 170      | 140    | 412      | 1224  |
| 1715 - 1730  | 106      | 436       | 25         | 191      | 159    | 448      | 1365  |
| Period End   | 1093     | 4541      | 307        | 1799     | 1469   | 4239     | 13448 |
|              | NO       | RTH       | SO         | UTH      |        |          |       |
|              |          | ville Rd  | WE<br>Oxfo | -        | Woody  |          |       |
| Peak Per     | R        | T         | L          | <u>R</u> | Ŀ      | T        | TOTAL |
| 1430 - 1530  | 280      | 1397      | 113        | 563      | 402    | 1320     | 4075  |
| 1445 - 1545  | 301      | 1447      | 109        | 589      | 405    | 1366     | 4217  |
| 1500 - 1600  | 347      | 1517      | 95         | 601      | 434    | 1424     | 4418  |
| 1515 - 1615  | 368      | 1547      | 96         | 559      | 456    | 1435     | 4461  |
| 1530 - 1630  | 409      | 1556      | 93         | 576      | 491    | 1412     | 4537  |
| 1545 - 1645  | 409      | 1589      | 96         | 561      | 529    | 1425     | 4609  |
| 1600 - 1700  | 386      | 1591      | 98         | 582      | 546    | 1373     | 4576  |
| 1615 - 1715  | 402      | 1569      | 98         | 620      | 562    | 1405     | 4656  |
| 1630 - 1730  | 404      | 1588      | 101        | 660      | 576    | 1507     | 4836  |
| PEAK HR      | 404      | 1588      | 101        | 660      | 576    | 1507     | 4836  |
|              |          |           |            |          | W      | oodvill  |       |
|              |          | PEAK      | HOUR       |          | ▲      |          | 1992  |
|              |          | 1630 ·    | - 1730     |          | 1608   |          | ↓     |
|              |          |           |            |          | 404    |          | 1588  |
|              |          | Oxfo      | rd St      |          |        |          | ¥     |
|              | 761      |           |            |          |        |          | •     |
|              |          |           | 101        |          |        | ~        |       |
|              |          |           | 101        |          |        |          |       |
|              |          |           | 660        |          |        |          |       |
|              | 761      | Oxfo<br>→ | ord St     |          | 404    | ~        | 1366  |

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Woodville Rd

576

2083

1507

2248

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## R.O.A.R. DATA

Reliable, Original & Authentic Results

Ph.88196847, Fax 88196849, Mob.0418-239019

| All Vehicles | NO                | RTH          | WE  | EST      | SO    | JTH      |       |
|--------------|-------------------|--------------|-----|----------|-------|----------|-------|
|              | Woodv             | Woodville Rd |     | ord St   | Woodv | ville Rd |       |
| Time Per     | <u>T</u> <u>R</u> |              | L   | <u>R</u> | L     | Ī        | TOTAL |
| 1100 - 1115  | 217               | 75           | 31  | 175      | 93    | 288      | 879   |
| 1115 - 1130  | 329               | 68           | 30  | 115      | 86    | 325      | 953   |
| 1130 - 1145  | 298               | 69           | 29  | 174      | 91    | 347      | 1008  |
| 1145 - 1200  | 325               | 73           | 41  | 152      | 71    | 291      | 953   |
| 1200 - 1215  | 347               | 95           | 33  | 157      | 105   | 298      | 1035  |
| 1215 - 1230  | 350               | 82           | 30  | 130      | 115   | 299      | 1006  |
| 1230 - 1245  | 283               | 91           | 37  | 136      | 90    | 305      | 942   |
| 1245 - 1300  | 377               | 104          | 30  | 132      | 87    | 315      | 1045  |
| Period End   | 2526              | 657          | 261 | 1171     | 738   | 2468     | 7821  |

|             | NO           | RTH | WE   | ST    | SO    | UTH      |       |
|-------------|--------------|-----|------|-------|-------|----------|-------|
|             | Woodville Rd |     | Oxfo | rd St | Woodv | ville Rd |       |
| Peak Per    | Ţ            | R   | L    | R     | L     | <u>T</u> | TOTAL |
| 1100 - 1200 | 1169         | 285 | 131  | 616   | 341   | 1251     | 3793  |
| 1115 - 1215 | 1299         | 305 | 133  | 598   | 353   | 1261     | 3949  |
| 1130 - 1230 | 1320         | 319 | 133  | 613   | 382   | 1235     | 4002  |
| 1145 - 1245 | 1305         | 341 | 141  | 575   | 381   | 1193     | 3936  |
| 1200 - 1300 | 1357         | 372 | 130  | 555   | 397   | 1217     | 4028  |



#### **R.O.A.R. DATA** *Reliable, Original & Authentic Results*

Ph.88196847, Fax 88196849, Mob.0418-239019

| All Vehicles | WE   | ST       | NO       | RTH    | EA       | ST       |       |
|--------------|------|----------|----------|--------|----------|----------|-------|
|              | Oxfo | rd St    | Highla   | nds St | Oxfo     | rd St    |       |
| Time Per     | L    | <u>T</u> | <u>R</u> | L      | <u>T</u> | <u>R</u> | TOTAL |
| 0730 - 0745  | 1    | 221      | 1        | 0      | 93       | 1        | 317   |
| 0745 - 0800  | 1    | 236      | 1        | 3      | 139      | 3        | 383   |
| 0800 - 0815  | 2    | 193      | 1        | 3      | 132      | 2        | 333   |
| 0815 - 0830  | 2    | 205      | 6        | 5      | 99       | 7        | 324   |
| 0830 - 0845  | 5    | 209      | 4        | 8      | 116      | 20       | 362   |
| 0845 - 0900  | 7    | 159      | 19       | 14     | 107      | 25       | 331   |
| 0900 - 0915  | 0    | 171      | 6        | 9      | 100      | 8        | 294   |
| 0915 - 0930  | 0    | 161      | 5        | 9      | 95       | 6        | 276   |
| Period End   | 18   | 1555     | 43       | 51     | 881      | 72       | 2620  |

|             | WEST      |          | NO       | RTH    | EA   | ST       |       |
|-------------|-----------|----------|----------|--------|------|----------|-------|
|             | Oxford St |          | Highla   | nds St | Oxfo | rd St    |       |
| Peak Per    | L         | <u>T</u> | <u>R</u> | L      | Ţ    | <u>R</u> | TOTAL |
| 0730 - 0830 | 6         | 855      | 9        | 11     | 463  | 13       | 1357  |
| 0745 - 0845 | 10        | 843      | 12       | 19     | 486  | 32       | 1402  |
| 0800 - 0900 | 16        | 766      | 30       | 30     | 454  | 54       | 1350  |
| 0815 - 0915 | 14        | 744      | 35       | 36     | 422  | 60       | 1311  |
| 0830 - 0930 | 12        | 700      | 34       | 40     | 418  | 59       | 1263  |







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| Road       | 01 Highland Street                 | Average Weekday | 485  |
|------------|------------------------------------|-----------------|------|
| Location   | approx. 50m north of Oxford Street | 7 Day Average   | 423  |
| Site No.   | 1                                  | Weekday Heavy's | 2.2% |
| Start Date | Saturday 9-May-15                  | 7 Day Heavy's   | 2.1% |
| Direction  | Combined                           |                 |      |

|           |        |        | [      | ay of Week | (      |       |        |       |       |
|-----------|--------|--------|--------|------------|--------|-------|--------|-------|-------|
|           | Mon    | Tue    | Wed    | Thu        | Fri    | Sat   | Sun    | Ave   | 7 Day |
| Time      | 11-May | 12-May | 13-May | 14-May     | 15-May | 9-May | 10-May | W'day | Ave   |
| AM Peak   | 108    | 108    | 98     | 93         | 102    | 31    | 20     |       |       |
| PM Peak   | 91     | 81     | 60     | 75         | 52     | 36    | 20     |       |       |
| 0:00      | 0      | 0      | 4      | 2          | 0      | 4     | 5      | 1     | 2     |
| 1:00      | 0      | 0      | 0      | 0          | 0      | 2     | 4      | 0     | 1     |
| 2:00      | 0      | 0      | 0      | 1          | 0      | 1     | 2      | 0     | 1     |
| 3:00      | 1      | 1      | 0      | 0          | 1      | 2     | 0      | 1     | 1     |
| 4:00      | 1      | 1      | 1      | 2          | 0      | 0     | 0      | 1     | 1     |
| 5:00      | 4      | 9      | 6      |            | 5      | 1     | 2      | 5     | 4     |
| 6:00      | 10     | 8      | 8      | 9          | 12     | 3     | 0      | 9     | 7     |
| 7:00      | 11     | 9      | 13     | 14         | 11     | 9     | 5      | 12    | 10    |
| 8:00      | 108    | 108    | 98     | 93         | 102    | 21    | 9      | 102   | 77    |
| 9:00      | 48     | 33     | 65     | 24         | 47     | 24    | 10     | 43    | 36    |
| 10:00     | 13     | 15     | 22     | 12         | 17     | 31    | 20     | 16    | 19    |
| 11:00     | 24     | 28     | 33     | 18         | 21     | 25    | 18     | 25    | 24    |
| 12:00     | 30     | 16     | 15     | 25         | 31     | 21    | 20     | 23    | 23    |
| 13:00     | 33     | 23     | 22     | 28         | 19     | 20    | 20     | 25    | 24    |
| 14:00     | 65     | 34     | 42     | 48         | 45     | 16    | 19     | 47    | 38    |
| 15:00     | 91     | 81     | 60     | 75         | 52     | 36    | 20     | 72    | 59    |
| 16:00     | 26     | 12     | 38     | 19         | 15     | 13    | 17     | 22    | 20    |
| 17:00     | 22     | 12     | 34     | 26         | 21     | 26    | 12     | 23    | 22    |
| 18:00     | 19     | 22     | 23     | 22         | 13     | 17    | 11     | 20    | 18    |
| 19:00     | 11     | 17     | 9      | 12         | 10     | 6     | 12     | 12    | 11    |
| 20:00     | 10     | 11     | 4      | 8          | 9      | 6     | 11     | 8     | 8     |
| 21:00     | 10     | 8      | 10     | 7          | 12     | 9     | 4      | 9     | 9     |
| 22:00     | 3      | 3      | 8      | 10         | 3      | 4     | 8      | 5     | 6     |
| 23:00     | 1      | 0      | 1      | 3          | 10     | 4     | 5      | 3     | 3     |
| Total     | 541    | 451    | 516    | 460        | 456    | 301   | 234    | 485   | 423   |
| % Heavies | 1.8%   | 3.1%   | 1.4%   | 1.3%       | 3.5%   | 1.3%  | 2.1%   | 2.2%  | 2.1%  |



Appendix B

SIDRA INTERSECTION Results





Woodville Road / Lansdowne Street AM Peak Hour **Existing Conditions** Giveway / Yield (Two-Way)

| Moven    | nent Per  | formance - V   | <b>ehicles</b> |                    |                  |                     |                        |                      |                 |                        |                  |
|----------|-----------|----------------|----------------|--------------------|------------------|---------------------|------------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID   | Turn      | Demand<br>Flow | HV             | Deg.<br>Satn       | Average<br>Delay | Level of<br>Service | 95% Back o<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
| Coutbul  |           | veh/h          | %              | v/c                | sec              |                     | veh                    | m                    |                 | per veh                | km/h             |
| South: V | woodville | Rd - S Leg     |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 1        | L         | 34             | 5.0            | 0.473              | 8.4              | LOS A               | 0.0                    | 0.0                  | 0.00            | 1.08                   | 49.0             |
| 2        | Т         | 1753           | 5.0            | 0.473              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| Approa   | ch        | 1786           | 5.0            | 0.473              | 0.2              | NA                  | 0.0                    | 0.0                  | 0.00            | 0.02                   | 59.7             |
| North: V | Voodville | Rd - N Leg     |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 8        | Т         | 1316           | 5.0            | 0.301              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| 9        | R         | 33             | 5.0            | 0.232              | 37.0             | LOS C               | 0.7                    | 5.4                  | 0.92            | 0.99                   | 29.8             |
| Approa   | ch        | 1348           | 5.0            | 0.301              | 0.9              | NA                  | 0.7                    | 5.4                  | 0.02            | 0.02                   | 58.6             |
| West: L  | ansdowne  | e St - W Leg   |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 10       | L         | 23             | 5.0            | 0.241              | 48.7             | LOS D               | 0.7                    | 5.2                  | 0.94            | 1.00                   | 25.7             |
| 12       | R         | 16             | 5.0            | 1.000 <sup>4</sup> | 501.4            | LOS F               | 3.2                    | 23.4                 | 1.00            | 1.13                   | 4.0              |
| Approa   | ch        | 39             | 5.0            | 1.000              | 232.2            | LOS F               | 3.2                    | 23.4                 | 0.96            | 1.05                   | 8.1              |
| All Vehi | cles      | 3174           | 5.0            | 1.000              | 3.3              | NA                  | 3.2                    | 23.4                 | 0.02            | 0.03                   | 55.0             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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. 72

Woodville Road / Lansdowne Street PM Peak Hour **Existing Conditions** Giveway / Yield (Two-Way)

| Moven    | nent Per  | formance - V        | <b>ehicles</b> |                    |                  |                     |                        |                      |                 |                        |                  |
|----------|-----------|---------------------|----------------|--------------------|------------------|---------------------|------------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID   | Turn      | Demand<br>Flow      | HV             | Deg.<br>Satn       | Average<br>Delay | Level of<br>Service | 95% Back o<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
| South: \ | Moodvillo | veh/h<br>Rd - S Leg | %              | v/c                | sec              | _                   | veh                    | m                    | _               | per veh                | km/h             |
| South.   | voouville | 0                   |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 1        | L         | 32                  | 5.0            | 0.434              | 8.4              | LOS A               | 0.0                    | 0.0                  | 0.00            | 1.07                   | 49.0             |
| 2        | Т         | 1606                | 5.0            | 0.434              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| Approa   | ch        | 1638                | 5.0            | 0.434              | 0.2              | NA                  | 0.0                    | 0.0                  | 0.00            | 0.02                   | 59.7             |
| North: V | Noodville | Rd - N Leg          |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 8        | Т         | 1847                | 5.0            | 0.423              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| 9        | R         | 100                 | 5.0            | 0.532              | 38.1             | LOS C               | 2.1                    | 15.7                 | 0.93            | 1.07                   | 29.3             |
| Approa   | ch        | 1947                | 5.0            | 0.532              | 2.0              | NA                  | 2.1                    | 15.7                 | 0.05            | 0.06                   | 57.0             |
| West: L  | ansdowne  | e St - W Leg        |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 10       | L         | 35                  | 5.0            | 0.263              | 38.6             | LOS C               | 0.8                    | 6.1                  | 0.92            | 1.00                   | 29.1             |
| 12       | R         | 17                  | 5.0            | 1.000 <sup>4</sup> | 436.6            | LOS F               | 3.0                    | 21.8                 | 1.00            | 1.13                   | 4.6              |
| Approa   | ch        | 52                  | 5.0            | 1.000              | 168.5            | LOS F               | 3.0                    | 21.8                 | 0.94            | 1.04                   | 10.6             |
| All Vehi | cles      | 3637                | 5.0            | 1.000              | 3.5              | NA                  | 3.0                    | 21.8                 | 0.04            | 0.05                   | 54.7             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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. 72

Woodville Road / Lansdowne Street Sat Peak Hour **Existing Conditions** Giveway / Yield (Two-Way)

| Moven    | nent Per   | formance - V | /ehicles |                    |         |          |             |          |        |           |         |
|----------|------------|--------------|----------|--------------------|---------|----------|-------------|----------|--------|-----------|---------|
| May ID   | T          | Demand       |          | Deg.               | Average | Level of | 95% Back of |          | Prop.  | Effective | Average |
| Mov ID   | Turn       | Flow         | HV       | Satn               | Delay   | Service  | Vehicles    | Distance | Queued | Stop Rate | Speed   |
| Couth    | Maadvilla  | veh/h        | %        | v/c                | Sec     | _        | veh         | m        | _      | per veh   | km/h    |
|          | vvoouville | Rd - S Leg   |          |                    |         |          |             |          |        |           |         |
| 1        | L          | 34           | 5.0      | 0.413              | 8.4     | LOS A    | 0.0         | 0.0      | 0.00   | 1.07      | 49.0    |
| 2        | Т          | 1523         | 5.0      | 0.413              | 0.0     | LOS A    | 0.0         | 0.0      | 0.00   | 0.00      | 60.0    |
| Approa   | ch         | 1557         | 5.0      | 0.413              | 0.2     | NA       | 0.0         | 0.0      | 0.00   | 0.02      | 59.7    |
| North: \ | Noodville  | Rd - N Leg   |          |                    |         |          |             |          |        |           |         |
| 8        | Т          | 1613         | 5.0      | 0.369              | 0.0     | LOS A    | 0.0         | 0.0      | 0.00   | 0.00      | 60.0    |
| 9        | R          | 68           | 5.0      | 0.314              | 28.5    | LOS C    | 1.1         | 8.3      | 0.89   | 1.00      | 33.7    |
| Approa   | ch         | 1681         | 5.0      | 0.369              | 1.2     | NA       | 1.1         | 8.3      | 0.04   | 0.04      | 58.2    |
| West: L  | ansdowne   | e St - W Leg |          |                    |         |          |             |          |        |           |         |
| 10       | L          | 37           | 5.0      | 0.237              | 33.3    | LOS C    | 0.8         | 5.5      | 0.90   | 0.99      | 31.4    |
| 12       | R          | 22           | 5.0      | 1.000 <sup>4</sup> | 370.9   | LOS F    | 3.3         | 24.4     | 1.00   | 1.17      | 5.3     |
| Approa   | ch         | 59           | 5.0      | 1.000              | 159.9   | LOS F    | 3.3         | 24.4     | 0.94   | 1.05      | 11.1    |
| All Vehi | icles      | 3297         | 5.0      | 1.000              | 3.5     | NA       | 3.3         | 24.4     | 0.04   | 0.05      | 54.7    |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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. 72 INTERSECTION

Woodville Road / Lansdowne Street PM Peak Hour Post Development Giveway / Yield (Two-Way)

| Moven    | nent Per  | ormance - V         | ehicles |                    |                  |                     |                        |                      |                 |                        |                  |
|----------|-----------|---------------------|---------|--------------------|------------------|---------------------|------------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID   | Turn      | Demand<br>Flow      | ΗV      | Deg.<br>Satn       | Average<br>Delay | Level of<br>Service | 95% Back o<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
| South:   | Woodville | veh/h<br>Rd - S Leg | %       | V/C                | sec              | _                   | veh                    | m                    | _               | per veh                | km/h             |
| 1        | L         | 57                  | 5.0     | 0.460              | 8.4              | LOS A               | 0.0                    | 0.0                  | 0.00            | 1.06                   | 49.0             |
| 2        | Т         | 1679                | 5.0     | 0.460              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| Approa   | ch        | 1736                | 5.0     | 0.460              | 0.3              | NA                  | 0.0                    | 0.0                  | 0.00            | 0.03                   | 59.6             |
| North: V | Voodville | Rd - N Leg          |         |                    |                  |                     |                        |                      |                 |                        |                  |
| 8        | Т         | 1967                | 5.0     | 0.450              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| 9        | R         | 100                 | 5.0     | 0.642              | 50.0             | LOS D               | 2.7                    | 19.5                 | 0.96            | 1.12                   | 25.3             |
| Approa   | ch        | 2067                | 5.0     | 0.642              | 2.4              | NA                  | 2.7                    | 19.5                 | 0.05            | 0.05                   | 56.3             |
| West: L  | ansdowne  | e St - W Leg        |         |                    |                  |                     |                        |                      |                 |                        |                  |
| 10       | L         | 54                  | 5.0     | 0.487              | 53.5             | LOS D               | 1.6                    | 12.0                 | 0.95            | 1.05                   | 24.3             |
| 12       | R         | 17                  | 5.0     | 1.000 <sup>4</sup> | 423.8            | LOS F               | 2.9                    | 21.1                 | 1.00            | 1.13                   | 4.7              |
| Approa   | ch        | 71                  | 5.0     | 1.000              | 141.9            | LOS F               | 2.9                    | 21.1                 | 0.96            | 1.07                   | 12.2             |
| All Vehi | cles      | 3874                | 5.0     | 1.000              | 4.0              | NA                  | 2.9                    | 21.1                 | 0.04            | 0.06                   | 54.1             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

4 x = 1.00 due to minimum capacity

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Woodville Road / Lansdowne Street Sat Peak Hour Post Development Giveway / Yield (Two-Way)

| Moven    | nent Per  | formance - V        | /ehicles |                    |         |          |             |          |        |           |         |
|----------|-----------|---------------------|----------|--------------------|---------|----------|-------------|----------|--------|-----------|---------|
| May ID   | Turn      | Demand              | HV       | Deg.               | Average | Level of | 95% Back of |          | Prop.  | Effective | Average |
| Mov ID   | Turn      | Flow                |          | Satn               | Delay   | Service  | Vehicles    | Distance | Queued | Stop Rate | Speed   |
| South: 1 | Woodville | veh/h<br>Rd - S Leg | %        | v/c                | sec     |          | veh         | m        |        | per veh   | km/h    |
|          | · · · · · | 0                   |          |                    |         |          |             |          |        |           |         |
| 1        | L         | 62                  | 5.0      | 0.451              | 8.4     | LOS A    | 0.0         | 0.0      | 0.00   | 1.05      | 49.0    |
| 2        | Т         | 1637                | 5.0      | 0.451              | 0.0     | LOS A    | 0.0         | 0.0      | 0.00   | 0.00      | 60.0    |
| Approa   | ch        | 1699                | 5.0      | 0.451              | 0.3     | NA       | 0.0         | 0.0      | 0.00   | 0.04      | 59.5    |
| North: \ | Noodville | Rd - N Leg          |          |                    |         |          |             |          |        |           |         |
| 8        | Т         | 1726                | 5.0      | 0.395              | 0.0     | LOS A    | 0.0         | 0.0      | 0.00   | 0.00      | 60.0    |
| 9        | R         | 68                  | 5.0      | 0.409              | 37.3    | LOS C    | 1.5         | 10.8     | 0.93   | 1.03      | 29.6    |
| Approa   | ch        | 1795                | 5.0      | 0.409              | 1.4     | NA       | 1.5         | 10.8     | 0.04   | 0.04      | 57.8    |
| West: L  | ansdowne  | e St - W Leg        |          |                    |         |          |             |          |        |           |         |
| 10       | L         | 65                  | 5.0      | 0.544              | 52.7    | LOS D    | 1.9         | 14.1     | 0.95   | 1.07      | 24.5    |
| 12       | R         | 22                  | 5.0      | 1.000 <sup>4</sup> | 356.2   | LOS F    | 3.2         | 23.5     | 1.00   | 1.16      | 5.5     |
| Approa   | ch        | 87                  | 5.0      | 1.000              | 129.5   | LOS F    | 3.2         | 23.5     | 0.96   | 1.09      | 13.1    |
| All Vehi | icles     | 3581                | 5.0      | 1.000              | 4.0     | NA       | 3.2         | 23.5     | 0.04   | 0.06      | 54.0    |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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Woodville Road / Kimberley Street **Existing Conditions** AM Peak Hour

Giveway / Yield (Two-Way)

| Movem     | nent Per   | formance - V            | /ehicles |                     |                         |                     |                               |                           |                 |                                   |                          |
|-----------|------------|-------------------------|----------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|
| Mov ID    | Turn       | Demand<br>Flow<br>veh/h | HV<br>%  | Deg.<br>Satn<br>v/c | Average<br>Delay<br>sec | Level of<br>Service | 95% Back o<br>Vehicles<br>veh | of Queue<br>Distance<br>m | Prop.<br>Queued | Effective<br>Stop Rate<br>per veh | Average<br>Speed<br>km/h |
| South: V  | Voodville  | Rd - S Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 2         | Т          | 1818                    | 5.0      | 0.481               | 0.0                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| Approad   | h          | 1818                    | 5.0      | 0.481               | 0.0                     | NA                  | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| East: Ki  | mberley \$ | St - E Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 4         | L          | 32                      | 5.0      | 0.086               | 18.2                    | LOS B               | 0.3                           | 2.2                       | 0.81            | 0.94                              | 40.1                     |
| Approad   | h          | 32                      | 5.0      | 0.086               | 18.2                    | LOS B               | 0.3                           | 2.2                       | 0.81            | 0.94                              | 40.1                     |
| North: V  | Voodville  | Rd - N Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 7         | L          | 2                       | 5.0      | 0.354               | 8.4                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 1.10                              | 49.0                     |
| 8         | Т          | 1336                    | 5.0      | 0.354               | 0.0                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| Approac   | h          | 1338                    | 5.0      | 0.354               | 0.0                     | NA                  | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| All Vehic | cles       | 3187                    | 5.0      | 0.481               | 0.2                     | NA                  | 0.3                           | 2.2                       | 0.01            | 0.01                              | 59.7                     |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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Woodville Road / Kimberley Street Existing Conditions PM Peak Hour

Giveway / Yield (Two-Way)

| Moven    | nent Per   | formance - V            | /ehicles |                     |                         |                     |                               |                           |                 |                                   |                          |
|----------|------------|-------------------------|----------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|
| Mov ID   | Turn       | Demand<br>Flow<br>veh/h | HV<br>%  | Deg.<br>Satn<br>v/c | Average<br>Delay<br>sec | Level of<br>Service | 95% Back o<br>Vehicles<br>veh | of Queue<br>Distance<br>m | Prop.<br>Queued | Effective<br>Stop Rate<br>per veh | Average<br>Speed<br>km/h |
| South: \ | Woodville  | Rd - S Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 2        | Т          | 1621                    | 5.0      | 0.429               | 0.0                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| Approa   | ch         | 1621                    | 5.0      | 0.429               | 0.0                     | NA                  | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| East: Ki | imberley S | St - E Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 4        | L          | 92                      | 5.0      | 0.776               | 82.4                    | LOS F               | 3.4                           | 24.5                      | 0.98            | 1.17                              | 18.4                     |
| Approa   | ch         | 92                      | 5.0      | 0.776               | 82.4                    | LOS F               | 3.4                           | 24.5                      | 0.98            | 1.17                              | 18.4                     |
| North: V | Noodville  | Rd - N Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 7        | L          | 15                      | 5.0      | 0.508               | 8.4                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 1.09                              | 49.0                     |
| 8        | Т          | 1904                    | 5.0      | 0.508               | 0.0                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| Approa   | ch         | 1919                    | 5.0      | 0.508               | 0.1                     | NA                  | 0.0                           | 0.0                       | 0.00            | 0.01                              | 59.9                     |
| All Vehi | icles      | 3632                    | 5.0      | 0.776               | 2.1                     | NA                  | 3.4                           | 24.5                      | 0.02            | 0.03                              | 56.7                     |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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Woodville Road / Kimberley Street **Existing Conditions** Sat Peak Hour

Giveway / Yield (Two-Way)

| Mover    | nent Per   | formance - V            | /ehicles |                     |                         |                     |                               |                           |                 |                                   |                          |
|----------|------------|-------------------------|----------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|
| Mov ID   | Turn       | Demand<br>Flow<br>veh/h | HV<br>%  | Deg.<br>Satn<br>v/c | Average<br>Delay<br>sec | Level of<br>Service | 95% Back o<br>Vehicles<br>veh | of Queue<br>Distance<br>m | Prop.<br>Queued | Effective<br>Stop Rate<br>per veh | Average<br>Speed<br>km/h |
| South: \ | Noodville  | Rd - S Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 2        | Т          | 1555                    | 5.0      | 0.412               | 0.0                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| Approad  | ch         | 1555                    | 5.0      | 0.412               | 0.0                     | NA                  | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| East: Ki | mberley \$ | St - E Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 4        | L          | 61                      | 5.0      | 0.283               | 28.9                    | LOS C               | 1.0                           | 7.4                       | 0.91            | 1.00                              | 33.5                     |
| Approad  | ch         | 61                      | 5.0      | 0.283               | 28.9                    | LOS C               | 1.0                           | 7.4                       | 0.91            | 1.00                              | 33.5                     |
| North: V | Voodville  | Rd - N Leg              |          |                     |                         |                     |                               |                           |                 |                                   |                          |
| 7        | L          | 8                       | 5.0      | 0.433               | 8.4                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 1.10                              | 49.0                     |
| 8        | Т          | 1628                    | 5.0      | 0.433               | 0.0                     | LOS A               | 0.0                           | 0.0                       | 0.00            | 0.00                              | 60.0                     |
| Approad  | ch         | 1637                    | 5.0      | 0.433               | 0.0                     | NA                  | 0.0                           | 0.0                       | 0.00            | 0.01                              | 59.9                     |
| All Vehi | cles       | 3253                    | 5.0      | 0.433               | 0.6                     | NA                  | 1.0                           | 7.4                       | 0.02            | 0.02                              | 59.1                     |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

Processed: Tuesday, 19 May 2015 4:03:27 PM SIDRA INTERSECTION 5.1.13.2093 Project: P:\15S1300-1399\15S1396000 258-264 Woodville Rd, Merrylands - John Cootes Site\Modelling \150519sid-15S1396000-Kimberley St.sip 8000056, GTA CONSULTANTS, ENTERPRISE

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Woodville Road / Kimberley Street Post Development PM Peak Hour

Signals - Fixed Time Cycle Time = 145 seconds (User-Given Cycle Time)

| Moven    | nent P <u>er</u> f | ormance - V             | /ehicle <u>s</u> |                     |                         |                     |                               |                           |                 |                                   |                          |
|----------|--------------------|-------------------------|------------------|---------------------|-------------------------|---------------------|-------------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|
| Mov ID   | Turn               | Demand<br>Flow<br>veh/h | HV<br>%          | Deg.<br>Satn<br>v/c | Average<br>Delay<br>sec | Level of<br>Service | 95% Back o<br>Vehicles<br>veh | of Queue<br>Distance<br>m | Prop.<br>Queued | Effective<br>Stop Rate<br>per veh | Average<br>Speed<br>km/h |
| South:   | Woodville          | Rd - S Leg              | /0               | v/C                 | 366                     |                     | Ven                           | 111                       |                 | per veri                          | KII1/11                  |
| 1        | L                  | 225                     | 5.0              | 0.812               | 10.9                    | LOS A               | 12.7                          | 92.9                      | 0.24            | 0.88                              | 47.0                     |
| 2        | Т                  | 1564                    | 5.0              | 0.812               | 2.9                     | LOS A               | 14.2                          | 104.0                     | 0.24            | 0.23                              | 54.2                     |
| Approa   | ch                 | 1789                    | 5.0              | 0.812               | 3.9                     | LOS A               | 14.2                          | 104.0                     | 0.24            | 0.31                              | 53.2                     |
| East: K  | imberley S         | St - E Leg              |                  |                     |                         |                     |                               |                           |                 |                                   |                          |
| 4        | L                  | 92                      | 5.0              | 0.379               | 61.9                    | LOS E               | 8.2                           | 60.2                      | 0.91            | 0.81                              | 22.4                     |
| 5        | Т                  | 22                      | 5.0              | 0.379               | 53.5                    | LOS D               | 8.2                           | 60.2                      | 0.91            | 0.74                              | 22.6                     |
| 6        | R                  | 21                      | 5.0              | 0.379               | 61.6                    | LOS E               | 8.2                           | 60.2                      | 0.91            | 0.80                              | 22.4                     |
| Approa   | ch                 | 135                     | 5.0              | 0.379               | 60.5                    | LOS E               | 8.2                           | 60.2                      | 0.91            | 0.79                              | 22.4                     |
| North: \ | Noodville          | Rd - N Leg              |                  |                     |                         |                     |                               |                           |                 |                                   |                          |
| 7        | L                  | 15                      | 5.0              | 0.457               | 10.4                    | LOS A               | 3.9                           | 28.8                      | 0.10            | 1.07                              | 47.3                     |
| 8        | Т                  | 1822                    | 5.0              | 0.457               | 2.5                     | LOS A               | 4.0                           | 28.8                      | 0.13            | 0.12                              | 55.4                     |
| 9        | R                  | 202                     | 5.0              | 0.804               | 29.4                    | LOS C               | 7.3                           | 53.6                      | 0.65            | 0.86                              | 33.3                     |
| Approa   | ch                 | 2039                    | 5.0              | 0.804               | 5.2                     | LOS A               | 7.3                           | 53.6                      | 0.18            | 0.20                              | 52.0                     |
| West: F  | RoadName           | ;                       |                  |                     |                         |                     |                               |                           |                 |                                   |                          |
| 10       | L                  | 155                     | 5.0              | 0.571               | 17.2                    | LOS B               | 6.3                           | 46.2                      | 0.70            | 0.81                              | 41.1                     |
| 11       | Т                  | 17                      | 5.0              | 0.571               | 9.2                     | LOS A               | 6.3                           | 46.2                      | 0.70            | 0.61                              | 43.2                     |
| 12       | R                  | 172                     | 5.0              | 0.799               | 79.3                    | LOS F               | 12.7                          | 93.1                      | 1.00            | 0.90                              | 18.9                     |
| Approa   | ch                 | 343                     | 5.0              | 0.799               | 47.9                    | LOS D               | 12.7                          | 93.1                      | 0.85            | 0.84                              | 25.9                     |
| All Vehi | cles               | 4306                    | 5.0              | 0.812               | 9.8                     | LOS A               | 14.2                          | 104.0                     | 0.28            | 0.31                              | 46.7                     |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model used.

| Moven   | nent Performance - | Pedestrian | S       |          |              |          |        |           |
|---------|--------------------|------------|---------|----------|--------------|----------|--------|-----------|
|         |                    | Demand     | Average | Level of | Average Back | of Queue | Prop.  | Effective |
| Mov ID  | Description        | Flow       | Delay   | Service  | Pedestrian   | Distance | Queued | Stop Rate |
|         |                    | ped/h      | sec     |          | ped          | m        |        | per ped   |
| P3      | Across E approach  | 53         | 7.6     | LOS A    | 0.1          | 0.1      | 0.32   | 0.32      |
| P5      | Across N approach  | 53         | 60.1    | LOS F    | 0.2          | 0.2      | 0.91   | 0.91      |
| P7      | Across W approach  | 53         | 13.7    | LOS B    | 0.1          | 0.1      | 0.43   | 0.43      |
| All Ped | estrians           | 159        | 27.1    | LOS C    |              |          | 0.56   | 0.56      |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

Processed: Friday, 5 June 2015 11:32:13 AM SIDRA INTERSECTION 5.1.13.2093 Project: P:\15S1300-1399\15S1396000 258-264 Woodville Rd, Merrylands - John Cootes Site\Modelling \150519sid-15S1396000-Kimberley St.sip 8000056, GTA CONSULTANTS, ENTERPRISE



Woodville Road / Kimberley Street Post Development Sat Peak Hour

Signals - Fixed Time Cycle Time = 145 seconds (User-Given Cycle Time)

| Moven    | nent P <u>er</u> | formance - V            | /ehicles |                     |                         |                     |                             |                           |                 |                                   |                          |
|----------|------------------|-------------------------|----------|---------------------|-------------------------|---------------------|-----------------------------|---------------------------|-----------------|-----------------------------------|--------------------------|
| Mov ID   | Turn             | Demand<br>Flow<br>veh/h | HV<br>%  | Deg.<br>Satn<br>v/c | Average<br>Delay<br>sec | Level of<br>Service | 95% Back<br>Vehicles<br>veh | of Queue<br>Distance<br>m | Prop.<br>Queued | Effective<br>Stop Rate<br>per veh | Average<br>Speed<br>km/h |
| South:   | Woodville        | Rd - S Leg              | /0       | v/C                 | 366                     |                     | Ven                         | 111                       |                 | per ven                           | KIII/11                  |
| 1        | L                | 260                     | 5.0      | 0.860               | 13.0                    | LOS A               | 16.7                        | 121.6                     | 0.30            | 0.88                              | 45.1                     |
| 2        | Т                | 1463                    | 5.0      | 0.860               | 5.1                     | LOS A               | 22.4                        | 163.7                     | 0.35            | 0.33                              | 50.9                     |
| Approa   | ch               | 1723                    | 5.0      | 0.860               | 6.3                     | LOS A               | 22.4                        | 163.7                     | 0.34            | 0.42                              | 49.9                     |
| East: Ki | imberley S       | St - E Leg              |          |                     |                         |                     |                             |                           |                 |                                   |                          |
| 4        | L                | 61                      | 5.0      | 0.243               | 53.6                    | LOS D               | 6.0                         | 43.9                      | 0.83            | 0.80                              | 24.5                     |
| 5        | Т                | 26                      | 5.0      | 0.243               | 45.2                    | LOS D               | 6.0                         | 43.9                      | 0.83            | 0.67                              | 25.0                     |
| 6        | R                | 21                      | 5.0      | 0.243               | 53.3                    | LOS D               | 6.0                         | 43.9                      | 0.83            | 0.79                              | 24.6                     |
| Approa   | ch               | 108                     | 5.0      | 0.243               | 51.5                    | LOS D               | 6.0                         | 43.9                      | 0.83            | 0.76                              | 24.6                     |
| North: V | Noodville        | Rd - N Leg              |          |                     |                         |                     |                             |                           |                 |                                   |                          |
| 7        | L                | 8                       | 5.0      | 0.432               | 13.7                    | LOS A               | 7.5                         | 54.8                      | 0.22            | 1.05                              | 44.6                     |
| 8        | Т                | 1508                    | 5.0      | 0.432               | 5.7                     | LOS A               | 7.5                         | 54.8                      | 0.23            | 0.21                              | 50.9                     |
| 9        | R                | 234                     | 5.0      | 0.973               | 83.0                    | LOS F               | 17.9                        | 130.3                     | 1.00            | 1.09                              | 18.3                     |
| Approa   | ch               | 1751                    | 5.0      | 0.973               | 16.1                    | LOS B               | 17.9                        | 130.3                     | 0.33            | 0.33                              | 41.1                     |
| West: F  | RoadName         | 9                       |          |                     |                         |                     |                             |                           |                 |                                   |                          |
| 10       | L                | 234                     | 5.0      | 0.801               | 28.3                    | LOS B               | 11.2                        | 81.6                      | 0.77            | 0.88                              | 34.1                     |
| 11       | Т                | 26                      | 5.0      | 0.801               | 20.3                    | LOS B               | 11.2                        | 81.6                      | 0.77            | 0.73                              | 35.2                     |
| 12       | R                | 260                     | 5.0      | 0.839               | 75.3                    | LOS F               | 19.6                        | 142.7                     | 1.00            | 0.93                              | 19.5                     |
| Approa   | ch               | 520                     | 5.0      | 0.839               | 51.4                    | LOS D               | 19.6                        | 142.7                     | 0.88            | 0.90                              | 24.9                     |
| All Vehi | icles            | 4102                    | 5.0      | 0.973               | 17.4                    | LOS B               | 22.4                        | 163.7                     | 0.42            | 0.45                              | 40.0                     |
|          |                  |                         |          |                     |                         |                     |                             |                           |                 |                                   |                          |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model used.

| Movement Performance - Pedestrians |                   |        |         |          |              |          |        |           |  |  |  |  |
|------------------------------------|-------------------|--------|---------|----------|--------------|----------|--------|-----------|--|--|--|--|
|                                    |                   | Demand | Average | Level of | Average Back | of Queue | Prop.  | Effective |  |  |  |  |
| Mov ID                             | Description       | Flow   | Delay   | Service  | Pedestrian   | Distance | Queued | Stop Rate |  |  |  |  |
|                                    |                   | ped/h  | sec     |          | ped          | m        |        | per ped   |  |  |  |  |
| P3                                 | Across E approach | 53     | 10.4    | LOS B    | 0.1          | 0.1      | 0.38   | 0.38      |  |  |  |  |
| P5                                 | Across N approach | 53     | 53.0    | LOS E    | 0.2          | 0.2      | 0.86   | 0.86      |  |  |  |  |
| P7                                 | Across W approach | 53     | 17.4    | LOS B    | 0.1          | 0.1      | 0.49   | 0.49      |  |  |  |  |
| All Pede                           | estrians          | 159    | 26.9    | LOS C    |              |          | 0.57   | 0.57      |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

Processed: Friday, 5 June 2015 11:32:29 AM SIDRA INTERSECTION 5.1.13.2093 Project: P:\15S1300-1399\15S1396000 258-264 Woodville Rd, Merrylands - John Cootes Site\Modelling \150519sid-15S1396000-Kimberley St.sip 8000056, GTA CONSULTANTS, ENTERPRISE



Woodville Road / Oxford Street Existing Conditions AM Peak Hour Signals - Fixed Time Cycle Time = 145 seconds (User-Given Cycle Time)

| Moven    | nent Per    | formance - V        | /ehicles |              |                  |                     |                        |          |                 |                        |                  |
|----------|-------------|---------------------|----------|--------------|------------------|---------------------|------------------------|----------|-----------------|------------------------|------------------|
| Mov ID   | Turn        | Demand<br>Flow      | HV       | Deg.<br>Satn | Average<br>Delay | Level of<br>Service | 95% Back (<br>Vehicles | Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
| South:   | Woodville   | veh/h<br>Rd - S Leg | %        | V/C          | Sec              | _                   | veh                    | m        | _               | per veh                | km/h             |
| 1        | L           | 331                 | 5.0      | 0.221        | 9.3              | LOS A               | 1.4                    | 10.5     | 0.07            | 0.68                   | 48.0             |
| 2        | Т           | 1704                | 5.0      | 0.909        | 36.2             | LOS C               | 56.4                   | 412.0    | 0.92            | 0.91                   | 28.8             |
| Approa   | ch          | 2035                | 5.0      | 0.909        | 31.8             | LOS C               | 56.4                   | 412.0    | 0.78            | 0.87                   | 30.8             |
| North: \ | Woodville   | Rd - N Leg          |          |              |                  |                     |                        |          |                 |                        |                  |
| 8        | Т           | 1189                | 5.0      | 0.507        | 8.4              | LOS A               | 12.2                   | 89.3     | 0.32            | 0.29                   | 47.6             |
| 9        | R           | 199                 | 5.0      | 0.899        | 93.3             | LOS F               | 15.7                   | 114.3    | 1.00            | 1.13                   | 16.8             |
| Approa   | ch          | 1388                | 5.0      | 0.899        | 20.5             | LOS B               | 15.7                   | 114.3    | 0.42            | 0.41                   | 37.7             |
| West: C  | Dxford St - | W Leg               |          |              |                  |                     |                        |          |                 |                        |                  |
| 10       | L           | 124                 | 5.0      | 0.906        | 71.7             | LOS F               | 33.5                   | 244.8    | 1.00            | 0.95                   | 20.2             |
| 12       | R           | 804                 | 5.0      | 0.906        | 74.4             | LOS F               | 38.1                   | 278.3    | 1.00            | 0.96                   | 19.7             |
| Approa   | ch          | 928                 | 5.0      | 0.906        | 74.0             | LOS F               | 38.1                   | 278.3    | 1.00            | 0.96                   | 19.8             |
| All Vehi | icles       | 4352                | 5.0      | 0.909        | 37.2             | LOS C               | 56.4                   | 412.0    | 0.71            | 0.75                   | 29.0             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model used.

| Movement Performance - Pedestrians |                   |                |                  |                     |                            |                      |                 |                        |  |  |  |  |
|------------------------------------|-------------------|----------------|------------------|---------------------|----------------------------|----------------------|-----------------|------------------------|--|--|--|--|
| Mov ID                             | Description       | Demand<br>Flow | Average<br>Delay | Level of<br>Service | Average Back<br>Pedestrian | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate |  |  |  |  |
|                                    |                   | ped/h          | sec              |                     | ped                        | m                    |                 | per ped                |  |  |  |  |
| P5                                 | Across N approach | 53             | 45.6             | LOS E               | 0.2                        | 0.2                  | 0.79            | 0.79                   |  |  |  |  |
| P7                                 | Across W approach | 53             | 22.1             | LOS C               | 0.1                        | 0.1                  | 0.55            | 0.55                   |  |  |  |  |
| All Pede                           | estrians          | 106            | 33.8             | LOS D               |                            |                      | 0.67            | 0.67                   |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

Processed: Thursday, 4 June 2015 12:55:20 PM SIDRA INTERSECTION 5.1.13.2093 Project: P:\15S1300-1399\15S1396000 258-264 Woodville Rd, Merrylands - John Cootes Site\Modelling \150519sid-15S1396000-Oxford St.sip 8000056, GTA CONSULTANTS, ENTERPRISE



Woodville Road / Oxford Street Existing Conditions PM Peak Hour Signals - Fixed Time Cycle Time = 145 seconds (User-Given Cycle Time)

| Moven    | nent Per    | formance - V   | /ehicles |              |                  |                     |                        |                      |                 |                        |                  |
|----------|-------------|----------------|----------|--------------|------------------|---------------------|------------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID   | Turn        | Demand<br>Flow | HV       | Deg.<br>Satn | Average<br>Delay | Level of<br>Service | 95% Back (<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
|          |             | veh/h          | %        | v/c          | sec              |                     | veh                    | m                    |                 | per veh                | km/h             |
| South:   | Woodville   | Rd - S Leg     |          |              |                  |                     |                        |                      |                 |                        |                  |
| 1        | L           | 606            | 5.0      | 0.481        | 10.8             | LOS A               | 4.7                    | 34.7                 | 0.12            | 0.70                   | 46.4             |
| 2        | Т           | 1525           | 5.0      | 0.944        | 55.4             | LOS D               | 59.9                   | 437.2                | 1.00            | 1.05                   | 22.9             |
| Approa   | ch          | 2132           | 5.0      | 0.944        | 42.7             | LOS D               | 59.9                   | 437.2                | 0.75            | 0.95                   | 26.7             |
| North: \ | Noodville   | Rd - N Leg     |          |              |                  |                     |                        |                      |                 |                        |                  |
| 8        | Т           | 1592           | 5.0      | 0.617        | 4.3              | LOS A               | 11.3                   | 82.3                 | 0.22            | 0.21                   | 52.6             |
| 9        | R           | 425            | 5.0      | 0.943        | 91.2             | LOS F               | 31.1                   | 226.7                | 1.00            | 1.19                   | 17.1             |
| Approa   | ch          | 2017           | 5.0      | 0.943        | 22.6             | LOS B               | 31.1                   | 226.7                | 0.39            | 0.41                   | 36.6             |
| West: C  | Dxford St - | W Leg          |          |              |                  |                     |                        |                      |                 |                        |                  |
| 10       | L           | 106            | 5.0      | 0.943        | 86.5             | LOS F               | 33.5                   | 244.8                | 1.00            | 0.98                   | 17.8             |
| 12       | R           | 695            | 5.0      | 0.943        | 89.6             | LOS F               | 34.1                   | 249.1                | 1.00            | 1.00                   | 17.3             |
| Approa   | ch          | 801            | 5.0      | 0.943        | 89.2             | LOS F               | 34.1                   | 249.1                | 1.00            | 0.99                   | 17.4             |
| All Vehi | icles       | 4949           | 5.0      | 0.944        | 42.1             | LOS C               | 59.9                   | 437.2                | 0.64            | 0.74                   | 27.4             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model used.

| Movement Performance - Pedestrians |                   |                |                  |                     |                            |                      |                 |                        |  |  |  |  |
|------------------------------------|-------------------|----------------|------------------|---------------------|----------------------------|----------------------|-----------------|------------------------|--|--|--|--|
| Mov ID                             | Description       | Demand<br>Flow | Average<br>Delay | Level of<br>Service | Average Back<br>Pedestrian | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate |  |  |  |  |
|                                    |                   | ped/h          | sec              |                     | ped                        | m                    |                 | per ped                |  |  |  |  |
| P5                                 | Across N approach | 53             | 53.0             | LOS E               | 0.2                        | 0.2                  | 0.86            | 0.86                   |  |  |  |  |
| P7                                 | Across W approach | 53             | 27.9             | LOS C               | 0.1                        | 0.1                  | 0.62            | 0.62                   |  |  |  |  |
| All Pede                           | estrians          | 106            | 40.5             | LOS E               |                            |                      | 0.74            | 0.74                   |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

Processed: Thursday, 4 June 2015 2:25:42 PM SIDRA INTERSECTION 5.1.13.2093 Project: P:\1551300-1399\1551396000 258-264 Woodville Rd, Merrylands - John Cootes Site\Modelling \150519sid-1551396000-Oxford St.sip 8000056, GTA CONSULTANTS, ENTERPRISE



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Woodville Road / Oxford Street **Existing Conditions** PM Peak Hour Signals - Fixed Time Cycle Time = 145 seconds (User-Given Cycle Time)

| Mover   | nent Per    | formance - V   | /ehicles |              |                  |                     |                      |                      |                 |                        |                  |
|---------|-------------|----------------|----------|--------------|------------------|---------------------|----------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID  | ) Turn      | Demand<br>Flow | HV       | Deg.<br>Satn | Average<br>Delay | Level of<br>Service | 95% Back<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
|         |             | veh/h          | %        | v/c          | sec              |                     | veh                  | m                    |                 | per veh                | km/h             |
| South:  | Woodville   | Rd - S Leg     |          |              |                  |                     |                      |                      |                 |                        |                  |
| 1       | L           | 418            | 5.0      | 0.325        | 10.0             | LOS A               | 2.1                  | 15.2                 | 0.08            | 0.69                   | 47.2             |
| 2       | Т           | 1428           | 5.0      | 0.857        | 35.9             | LOS C               | 43.4                 | 316.7                | 0.90            | 0.85                   | 28.9             |
| Approa  | ich         | 1846           | 5.0      | 0.857        | 30.0             | LOS C               | 43.4                 | 316.7                | 0.71            | 0.81                   | 31.7             |
| North:  | Woodville   | Rd - N Leg     |          |              |                  |                     |                      |                      |                 |                        |                  |
| 8       | Т           | 1319           | 5.0      | 0.511        | 3.8              | LOS A               | 7.7                  | 55.9                 | 0.18            | 0.17                   | 53.4             |
| 9       | R           | 392            | 5.0      | 0.861        | 71.4             | LOS F               | 24.9                 | 181.7                | 0.98            | 1.13                   | 20.2             |
| Approa  | ich         | 1711           | 5.0      | 0.861        | 19.3             | LOS B               | 24.9                 | 181.7                | 0.37            | 0.39                   | 38.9             |
| West: 0 | Oxford St - | W Leg          |          |              |                  |                     |                      |                      |                 |                        |                  |
| 10      | L           | 137            | 5.0      | 0.843        | 71.0             | LOS F               | 26.7                 | 195.3                | 1.00            | 0.92                   | 20.3             |
| 12      | R           | 584            | 5.0      | 0.843        | 71.7             | LOS F               | 26.7                 | 195.3                | 1.00            | 0.92                   | 20.2             |
| Approa  | ich         | 721            | 5.0      | 0.843        | 71.6             | LOS F               | 26.7                 | 195.3                | 1.00            | 0.92                   | 20.2             |
| All Veh | icles       | 4278           | 5.0      | 0.861        | 32.7             | LOS C               | 43.4                 | 316.7                | 0.62            | 0.66                   | 31.0             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model used.

| Movement Performance - Pedestrians |                   |                |                  |                     |                            |                      |                 |                        |  |  |  |  |
|------------------------------------|-------------------|----------------|------------------|---------------------|----------------------------|----------------------|-----------------|------------------------|--|--|--|--|
| Mov ID                             | Description       | Demand<br>Flow | Average<br>Delay | Level of<br>Service | Average Back<br>Pedestrian | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate |  |  |  |  |
|                                    |                   | ped/h          | sec              |                     | ped                        | m                    |                 | per ped                |  |  |  |  |
| P5                                 | Across N approach | 53             | 53.0             | LOS E               | 0.2                        | 0.2                  | 0.86            | 0.86                   |  |  |  |  |
| P7                                 | Across W approach | 53             | 26.7             | LOS C               | 0.1                        | 0.1                  | 0.61            | 0.61                   |  |  |  |  |
| All Pede                           | estrians          | 106            | 39.9             | LOS D               |                            |                      | 0.73            | 0.73                   |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Woodville Road / Lansdowne Street PM Peak Hour Post Development Giveway / Yield (Two-Way)

| Moven    | nent Per   | formance - V   | <b>ehicles</b> |                    |                  |                     |                        |                      |                 |                        |                  |
|----------|------------|----------------|----------------|--------------------|------------------|---------------------|------------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID   | Turn       | Demand<br>Flow | HV             | Deg.<br>Satn       | Average<br>Delay | Level of<br>Service | 95% Back o<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
| Coutbul  | Meeduille. | veh/h          | %              | v/c                | sec              |                     | veh                    | m                    |                 | per veh                | km/h             |
| South: V | woodville  | Rd - S Leg     |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 1        | L          | 57             | 5.0            | 0.460              | 8.4              | LOS A               | 0.0                    | 0.0                  | 0.00            | 1.06                   | 49.0             |
| 2        | Т          | 1679           | 5.0            | 0.460              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| Approa   | ch         | 1736           | 5.0            | 0.460              | 0.3              | NA                  | 0.0                    | 0.0                  | 0.00            | 0.03                   | 59.6             |
| North: V | Noodville  | Rd - N Leg     |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 8        | Т          | 1967           | 5.0            | 0.450              | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| 9        | R          | 100            | 5.0            | 0.642              | 50.0             | LOS D               | 2.7                    | 19.5                 | 0.96            | 1.12                   | 25.3             |
| Approa   | ch         | 2067           | 5.0            | 0.642              | 2.4              | NA                  | 2.7                    | 19.5                 | 0.05            | 0.05                   | 56.3             |
| West: L  | ansdowne   | e St - W Leg   |                |                    |                  |                     |                        |                      |                 |                        |                  |
| 10       | L          | 54             | 5.0            | 0.487              | 53.5             | LOS D               | 1.6                    | 12.0                 | 0.95            | 1.05                   | 24.3             |
| 12       | R          | 17             | 5.0            | 1.000 <sup>4</sup> | 423.8            | LOS F               | 2.9                    | 21.1                 | 1.00            | 1.13                   | 4.7              |
| Approa   | ch         | 71             | 5.0            | 1.000              | 141.9            | LOS F               | 2.9                    | 21.1                 | 0.96            | 1.07                   | 12.2             |
| All Vehi | cles       | 3874           | 5.0            | 1.000              | 4.0              | NA                  | 2.9                    | 21.1                 | 0.04            | 0.06                   | 54.1             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

4 x = 1.00 due to minimum capacity

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- -----

Woodville Road / Oxford Street **Existing Conditions** PM Peak Hour Signals - Fixed Time Cycle Time = 145 seconds (User-Given Cycle Time)

| Mover   | nent Per    | formance - V   | /ehicles |              |                  |                     |                      |                      |                 |                        |                  |
|---------|-------------|----------------|----------|--------------|------------------|---------------------|----------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID  | Turn        | Demand<br>Flow | HV       | Deg.<br>Satn | Average<br>Delay | Level of<br>Service | 95% Back<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
|         |             | veh/h          | %        | v/c          | sec              |                     | veh                  | m                    |                 | per veh                | km/h             |
| South:  | Woodville   | Rd - S Leg     |          |              |                  |                     |                      |                      |                 |                        |                  |
| 1       | L           | 418            | 5.0      | 0.322        | 9.9              | LOS A               | 2.1                  | 15.1                 | 0.08            | 0.69                   | 47.3             |
| 2       | Т           | 1568           | 5.0      | 0.899        | 39.0             | LOS C               | 52.1                 | 380.0                | 0.93            | 0.91                   | 27.7             |
| Approa  | ich         | 1986           | 5.0      | 0.899        | 32.9             | LOS C               | 52.1                 | 380.0                | 0.75            | 0.87                   | 30.4             |
| North:  | Woodville   | Rd - N Leg     |          |              |                  |                     |                      |                      |                 |                        |                  |
| 8       | Т           | 1459           | 5.0      | 0.555        | 3.1              | LOS A               | 7.4                  | 54.2                 | 0.16            | 0.15                   | 54.5             |
| 9       | R           | 392            | 5.0      | 0.903        | 81.2             | LOS F               | 27.0                 | 197.4                | 1.00            | 1.16                   | 18.5             |
| Approa  | ich         | 1851           | 5.0      | 0.903        | 19.6             | LOS B               | 27.0                 | 197.4                | 0.34            | 0.36                   | 38.7             |
| West: 0 | Oxford St - | W Leg          |          |              |                  |                     |                      |                      |                 |                        |                  |
| 10      | L           | 137            | 5.0      | 0.894        | 80.0             | LOS F               | 28.9                 | 211.1                | 1.00            | 0.96                   | 18.8             |
| 12      | R           | 584            | 5.0      | 0.894        | 80.5             | LOS F               | 28.9                 | 211.1                | 1.00            | 0.96                   | 18.7             |
| Approa  | ich         | 721            | 5.0      | 0.894        | 80.4             | LOS F               | 28.9                 | 211.1                | 1.00            | 0.96                   | 18.7             |
| All Veh | icles       | 4558           | 5.0      | 0.903        | 35.0             | LOS C               | 52.1                 | 380.0                | 0.62            | 0.68                   | 30.0             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Intersection and Approach LOS values are based on average delay for all vehicle movements.

SIDRA Standard Delay Model used.

| Movement Performance - Pedestrians |                   |                |                  |                     |                            |                      |                 |                        |  |  |  |  |
|------------------------------------|-------------------|----------------|------------------|---------------------|----------------------------|----------------------|-----------------|------------------------|--|--|--|--|
| Mov ID                             | Description       | Demand<br>Flow | Average<br>Delay | Level of<br>Service | Average Back<br>Pedestrian | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate |  |  |  |  |
|                                    |                   | ped/h          | sec              |                     | ped                        | m                    |                 | per ped                |  |  |  |  |
| P5                                 | Across N approach | 53             | 54.7             | LOS E               | 0.2                        | 0.2                  | 0.87            | 0.87                   |  |  |  |  |
| P7                                 | Across W approach | 53             | 24.9             | LOS C               | 0.1                        | 0.1                  | 0.59            | 0.59                   |  |  |  |  |
| All Pede                           | estrians          | 106            | 39.8             | LOS D               |                            |                      | 0.73            | 0.73                   |  |  |  |  |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Oxford Street / Highland Street AM Peak Hour Existing Conditions Giveway / Yield (Two-Way)

| Moven    | nent Per    | ormance - V    | ehicles |              |                  |                     |                        |                      |                 |                        |                  |
|----------|-------------|----------------|---------|--------------|------------------|---------------------|------------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID   | Turn        | Demand<br>Flow | ΗV      | Deg.<br>Satn | Average<br>Delay | Level of<br>Service | 95% Back o<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
| East: 0  | xford St -  | veh/h          | %       | v/c          | sec              |                     | veh                    | m                    |                 | per veh                | km/h             |
| 5        | T           | 512            | 5.0     | 0.329        | 9.2              | LOS A               | 5.4                    | 39.8                 | 1.00            | 0.00                   | 44.1             |
|          |             |                |         |              |                  |                     |                        |                      |                 |                        |                  |
| 6        | R           | 34             | 5.0     | 0.329        | 17.9             | LOS B               | 5.4                    | 39.8                 | 1.00            | 1.08                   | 43.9             |
| Approa   | ch          | 545            | 5.0     | 0.329        | 9.8              | NA                  | 5.4                    | 39.8                 | 1.00            | 0.07                   | 44.1             |
| North: H | Highland S  | St - N Leg     |         |              |                  |                     |                        |                      |                 |                        |                  |
| 7        | L           | 20             | 5.0     | 0.125        | 21.4             | LOS B               | 0.4                    | 2.9                  | 0.82            | 0.94                   | 37.7             |
| 9        | R           | 13             | 5.0     | 0.125        | 21.7             | LOS B               | 0.4                    | 2.9                  | 0.82            | 0.95                   | 37.7             |
| Approa   | ch          | 33             | 5.0     | 0.125        | 21.5             | LOS B               | 0.4                    | 2.9                  | 0.82            | 0.94                   | 37.7             |
| West: C  | Dxford St - | W Leg          |         |              |                  |                     |                        |                      |                 |                        |                  |
| 10       | L           | 11             | 5.0     | 0.476        | 8.4              | LOS A               | 0.0                    | 0.0                  | 0.00            | 1.10                   | 49.0             |
| 11       | Т           | 887            | 5.0     | 0.476        | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| Approa   | ch          | 898            | 5.0     | 0.476        | 0.1              | NA                  | 0.0                    | 0.0                  | 0.00            | 0.01                   | 59.8             |
| All Vehi | icles       | 1476           | 5.0     | 0.476        | 4.1              | NA                  | 5.4                    | 39.8                 | 0.39            | 0.05                   | 52.3             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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Oxford Street / Highland Street PM Peak Hour Existing Conditions Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |             |                |     |              |                  |                     |                        |                      |                 |                        |                  |
|---------------------------------|-------------|----------------|-----|--------------|------------------|---------------------|------------------------|----------------------|-----------------|------------------------|------------------|
| Mov ID                          | Turn        | Demand<br>Flow | ΗV  | Deg.<br>Satn | Average<br>Delay | Level of<br>Service | 95% Back o<br>Vehicles | of Queue<br>Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
|                                 |             | veh/h          | %   | v/c          | sec              | 0011100             | veh                    | m                    | Quouou          | per veh                | km/h             |
| East: Oxford St - E Leg         |             |                |     |              |                  |                     |                        |                      |                 |                        |                  |
| 5                               | Т           | 1093           | 5.0 | 0.614        | 13.3             | LOS A               | 12.8                   | 93.8                 | 1.00            | 0.00                   | 40.9             |
| 6                               | R           | 25             | 5.0 | 0.614        | 21.9             | LOS B               | 12.8                   | 93.8                 | 1.00            | 1.28                   | 40.8             |
| Approach                        |             | 1118           | 5.0 | 0.614        | 13.5             | NA                  | 12.8                   | 93.8                 | 1.00            | 0.03                   | 40.9             |
| North: Highland St - N Leg      |             |                |     |              |                  |                     |                        |                      |                 |                        |                  |
| 7                               | L           | 19             | 5.0 | 0.101        | 23.1             | LOS B               | 0.3                    | 2.1                  | 0.81            | 0.92                   | 36.7             |
| 9                               | R           | 3              | 5.0 | 0.101        | 23.4             | LOS B               | 0.3                    | 2.1                  | 0.81            | 0.95                   | 36.7             |
| Approa                          | Approach    |                | 5.0 | 0.101        | 23.1             | LOS B               | 0.3                    | 2.1                  | 0.81            | 0.92                   | 36.7             |
| West: C                         | Oxford St - | W Leg          |     |              |                  |                     |                        |                      |                 |                        |                  |
| 10                              | L           | 3              | 5.0 | 0.414        | 8.4              | LOS A               | 0.0                    | 0.0                  | 0.00            | 1.10                   | 49.0             |
| 11                              | Т           | 778            | 5.0 | 0.414        | 0.0              | LOS A               | 0.0                    | 0.0                  | 0.00            | 0.00                   | 60.0             |
| Approa                          | ch          | 781            | 5.0 | 0.414        | 0.0              | NA                  | 0.0                    | 0.0                  | 0.00            | 0.00                   | 59.9             |
| All Vehicles                    |             | 1921           | 5.0 | 0.614        | 8.1              | NA                  | 12.8                   | 93.8                 | 0.59            | 0.03                   | 46.9             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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Oxford Street / Highland Street PM Peak Hour Post Development Giveway / Yield (Two-Way)

| Movement Performance - Vehicles |      |                |     |              |                  |                     |                      |          |                 |                        |                  |
|---------------------------------|------|----------------|-----|--------------|------------------|---------------------|----------------------|----------|-----------------|------------------------|------------------|
| Mov ID                          | Turn | Demand<br>Flow | HV  | Deg.<br>Satn | Average<br>Delay | Level of<br>Service | 95% Back<br>Vehicles | Distance | Prop.<br>Queued | Effective<br>Stop Rate | Average<br>Speed |
| East: Oxford St - E L           |      | veh/h          | %   | v/c          | sec              | _                   | veh                  | m        | _               | per veh                | km/h             |
|                                 |      | 0              | F 0 | 0.010        | 444              |                     | 12.0                 | 04.0     | 1.00            | 0.00                   | 40.2             |
| 5                               | Т    | 1093           | 5.0 | 0.616        | 14.1             | LOS A               | 13.0                 | 94.9     | 1.00            | 0.00                   | 40.3             |
| 6                               | R    | 25             | 5.0 | 0.616        | 22.8             | LOS B               | 13.0                 | 94.9     | 1.00            | 1.28                   | 40.1             |
| Approach                        |      | 1118           | 5.0 | 0.616        | 14.3             | NA                  | 13.0                 | 94.9     | 1.00            | 0.03                   | 40.3             |
| North: Highland St - N Leg      |      |                |     |              |                  |                     |                      |          |                 |                        |                  |
| 7                               | L    | 19             | 5.0 | 0.567        | 87.9             | LOS F               | 1.8                  | 13.1     | 0.96            | 1.09                   | 17.5             |
| 9                               | R    | 22             | 5.0 | 0.567        | 88.2             | LOS F               | 1.8                  | 13.1     | 0.96            | 1.06                   | 17.5             |
| Approach                        |      | 41             | 5.0 | 0.567        | 88.1             | LOS F               | 1.8                  | 13.1     | 0.96            | 1.07                   | 17.5             |
| West: Oxford St - W Leg         |      |                |     |              |                  |                     |                      |          |                 |                        |                  |
| 10                              | L    | 28             | 5.0 | 0.428        | 8.4              | LOS A               | 0.0                  | 0.0      | 0.00            | 1.08                   | 49.0             |
| 11                              | Т    | 778            | 5.0 | 0.428        | 0.0              | LOS A               | 0.0                  | 0.0      | 0.00            | 0.00                   | 60.0             |
| Approach                        |      | 806            | 5.0 | 0.428        | 0.3              | NA                  | 0.0                  | 0.0      | 0.00            | 0.04                   | 59.5             |
| All Vehicles                    |      | 1965           | 5.0 | 0.616        | 10.1             | NA                  | 13.0                 | 94.9     | 0.59            | 0.05                   | 45.0             |

Level of Service (LOS) Method: Delay (RTA NSW).

Vehicle movement LOS values are based on average delay per movement

Minor Road Approach LOS values are based on average delay for all vehicle movements.

NA: Intersection LOS and Major Road Approach LOS values are Not Applicable for two-way sign control since the average delay is not a good LOS measure due to zero delays associated with major road movements.

SIDRA Standard Delay Model used.

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